

Leach Testwork Confirms Ionic Clay REE Mineralisation at Tunas

Highlights

- **High-grade Ionic Absorption Clay (IAC) REE mineralisation confirmed at Tunas, as leach testwork has returned strong recovery of TREO and MREO**
- **Results include:**
 - Deeper sample group averaging 38% TREO recovery and 63% MREO recovery, with average recovered grades of approximately 951ppm TREO and 524ppm MREO;
 - Maximum calculated recoveries of 64% TREO and 104% MREO¹;
 - Multiple samples returning calculated MREO recoveries above 50%, including 66%, 65%, 71%, 76% and 104%, confirming strong leachability of the magnetic rare earth component within the tested weathered profile; and
 - Leach recoveries and recovered grades generally increasing toward the deeper parts of the auger holes, consistent with assay results and highlighting the potential for stronger mineralisation below the current limits of manual auger drilling.
- **Results support ongoing exploration at Tunas, with the next phase of work to include diamond drilling utilising man-portable drilling rigs to fully test the identified mineralisation**

Core Energy Minerals Limited (ASX:CR3) (“**Core Energy**”, “**CR3**” or the “**Company**”) is pleased to provide an update on results from infill auger sampling conducted across the Tunas Rare Earth Element (“**REE**”) Project in Paraná in Brazil.

Core Energy Minerals Managing Director, Tony Greenaway, said:

“We are extremely pleased with these first results from the leach testwork at Tunas. The results validate our planned on-going exploration at Tunas which will include moving to diamond drilling, enabling us to fully test the depth of the identified Ionic Absorption Clay hosted REE mineralisation.”

“Work to this point has been completed using low impact auger sampling equipment which has a depth limit of just 15 meters, so many of our holes have ended in high grade REE mineralisation. The use of man-portable diamond drilling will mean that we can fully test the complete clay profile at Tunas down to basement, and at the same time collect significant amounts of sample for more definitive metallurgical leach testwork.”

“We will continue to undertake staged exploration at Tunas as we advance the project toward an eventual maiden JORC mineral resource estimate.”

¹ MREO result above 100% interpreted as reflecting normal analytical and mass-balance variability rather than physical recovery above 100%

LEACHTESTWORK AT TUNAS CONFIRMS IAC MINERALISATION

Leach test work completed on auger samples from CR3's 100%-owned Tunas Project has returned highly encouraging results, supporting the recoverability of rare earth element mineralisation within the tested weathered profile. The results support the interpretation that both TREO and MREO mineralisation at Tunas are associated with ionic clay-style ("IAC") mineralisation within the weathered profile. The test work returned encouraging calculated recoveries, including an average Total Rare Earth Oxide ("TREO") recovery of approximately 38% and maximum TREO recovery of 64%, and an average Magnetic Rare Earth Oxide ("MREO") recovery of approximately 63% and maximum MREO recovery of 104% in the deeper sample group (Figure 1). Recoveries at or above 100% are interpreted to reflect normal analytical and mass-balance variability during sample preparation, assay and leach testing; and should not be interpreted as physical recoveries above 100%.

The leach tests were completed using ammonium sulphate, a widely used reagent for assessing the recoverable rare earth component in ionic clay systems. The results were achieved under mild conditions, at ambient temperature and low acidity, providing an encouraging indication that a meaningful portion of the rare earth mineralisation at Tunas is amenable to simple leach extraction conditions.

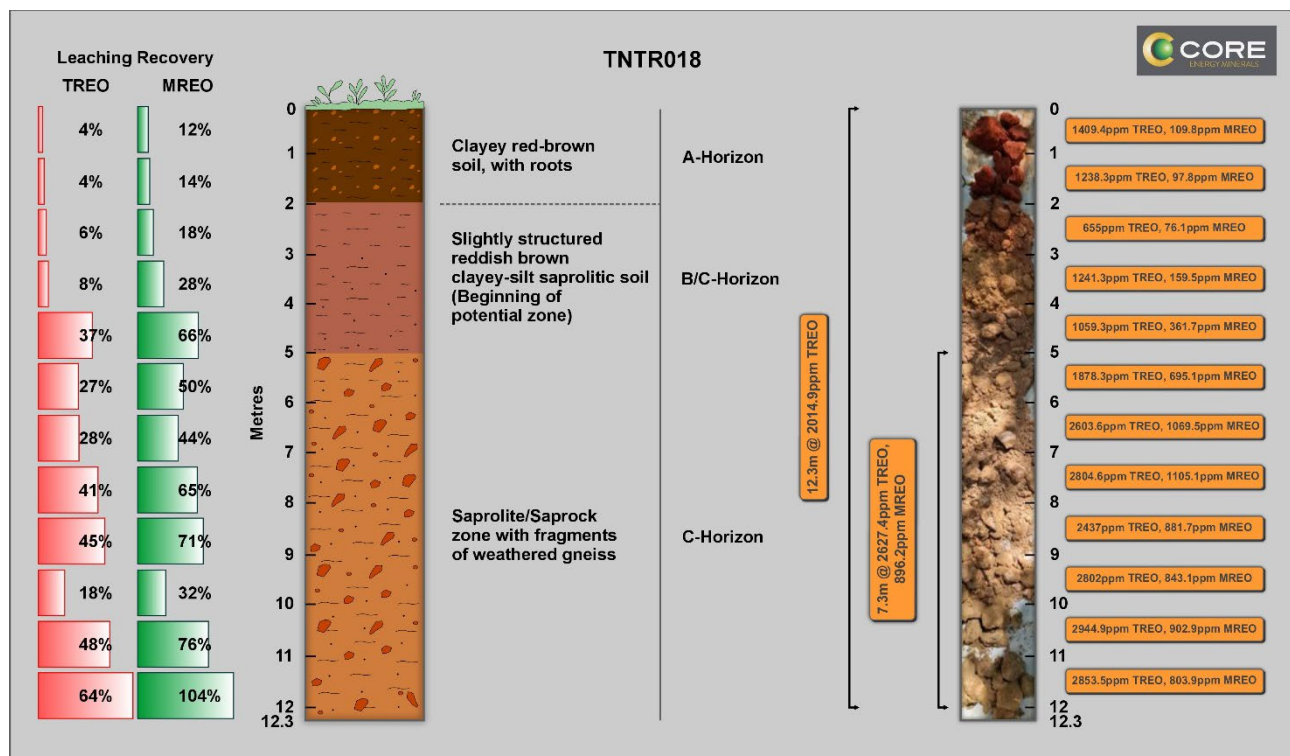


Figure 1: Representative auger hole profile for TNTR018 showing regolith horizons, lithological logging, assay intervals and calculated leach recoveries for TREO and MREO

Key results from this leach test include:

- Deeper sample group averaging **38%** TREO recovery and **63%** MREO recovery, with average recovered grades of approximately **951ppm** TREO and **524ppm** MREO;
- Maximum calculated recoveries of **64%** TREO and **104%** MREO, with the MREO result above 100% interpreted as reflecting normal analytical and mass-balance variability rather than physical recovery above 100%;

- Multiple samples returning calculated MREO recoveries above 50%, including **66%, 65%, 71%, 76% and 104%**, confirming strong leachability of the magnetic rare earth component within the tested weathered profile.

Consistent with the assay results, the leach test work shows a progressive increase in recovered rare earth content toward the deeper parts of the auger holes. This depth trend further supports the potential of the broader Tunas system, with lateral continuity, consistent mineralised thicknesses and elevated grades now complemented by encouraging metallurgical recoveries. The presence of recoverable MREO and yttrium adds further strategic value to the project.

The assay results have already demonstrated laterally continuous rare earth mineralisation over meaningful thicknesses and grades. The leach test results now provide an important additional layer of validation by confirming that a significant portion of the mineralisation is recoverable under weak leach conditions. Importantly, many intersections remain open at depth due to the limitations of manual auger drilling, which was not able to consistently test the full thickness of the weathered profile.

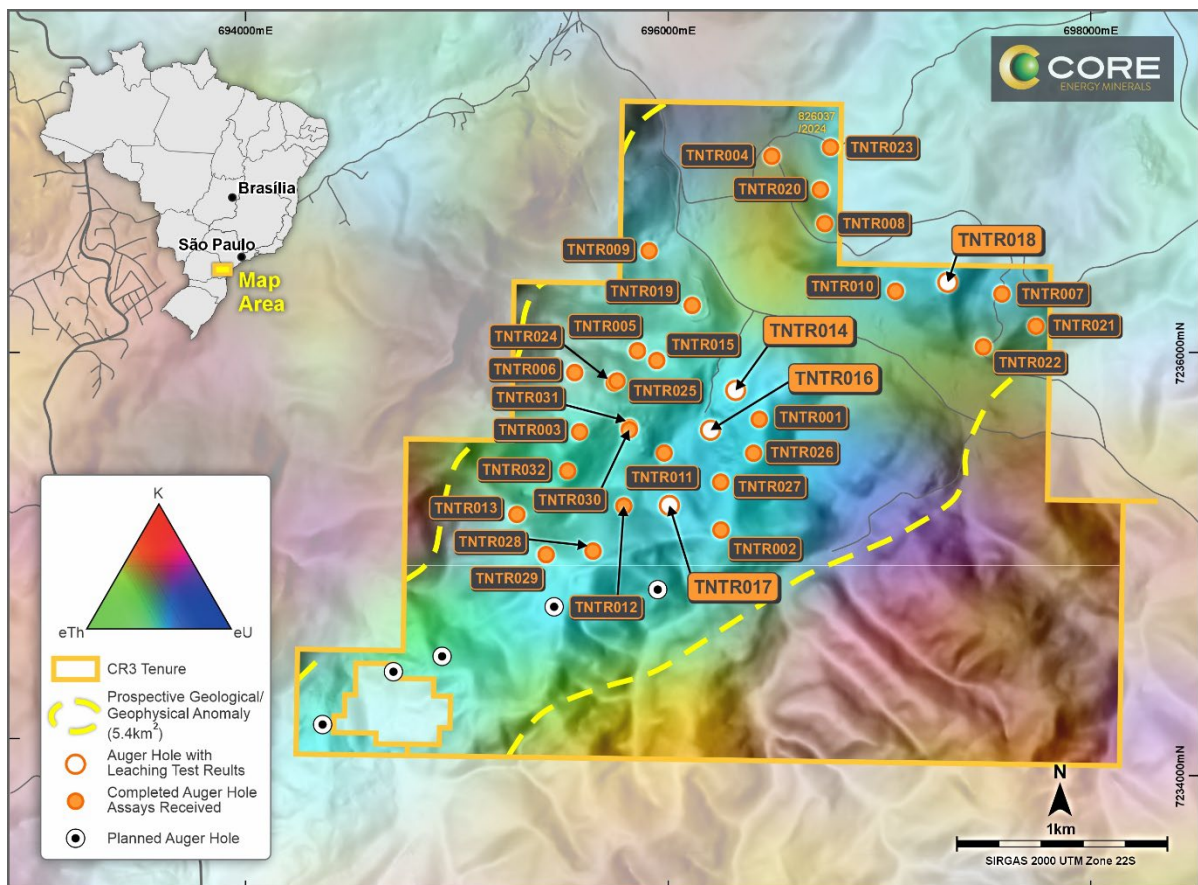


Figure 2: Location map of auger holes at the Tunas Rare Earths Project selected for leach test work.

The Company plans to undertake diamond drilling in the next phase of exploration, to test the full thickness of the weathered profile for IAC rare earths. Man-portable rigs may be utilised to access the rugged terrain and to minimise ground disturbance..

During the auger drilling program, selected samples from Tunas were submitted for additional size-fraction test work to assess whether screening could enhance rare earth grades within a finer sample fraction. The procedure included field screening at 2mm, preparation of the screened fraction to 80mesh in the laboratory, and direct chemical analysis. The results were compared against the corresponding bulk sample assays to evaluate whether the sieved fraction produced a systematic grade upgrade relative to the original sample.

As shown in **Figure 3** below, the bulk and sieved sample comparison does not demonstrate a clear or consistent enrichment trend in TREO grades following screening. The Sieved/Bulk curve varies above and below the zero baseline, irrespective of the absolute grade observed in each sample, indicating that the response is not controlled by grade and does not define a predictable upgrade pattern. This variable behaviour is interpreted to reflect the fine silty-clayey nature of the Tunas sample matrix, where the finer fraction is already dominant and is not materially separated by screening. As a result, the size-fraction test work is considered inconclusive as a method for systematically upgrading rare earth grades at Tunas, and the Company has elected to maintain its standard bulk sample analytical procedure as the most representative approach for ongoing evaluation.

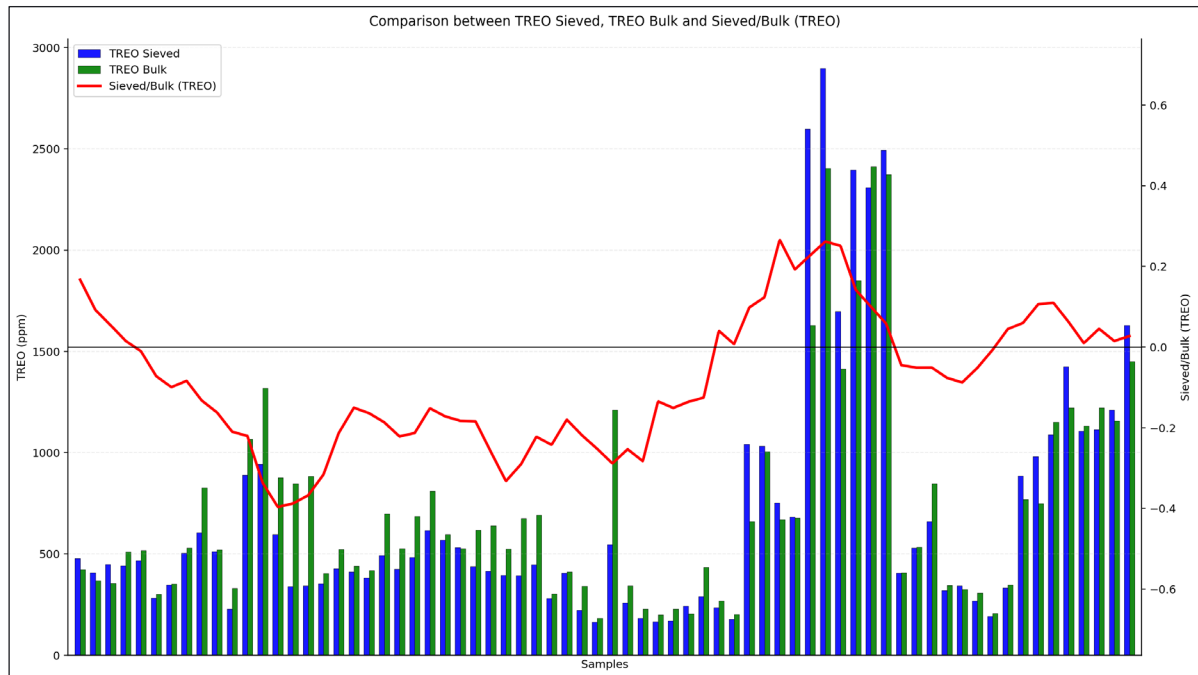


Figure 3: Comparison of TREO grades in bulk and sieved samples from Tunas, with the Sieved/Bulk curve showing the relative response of the screened fraction.

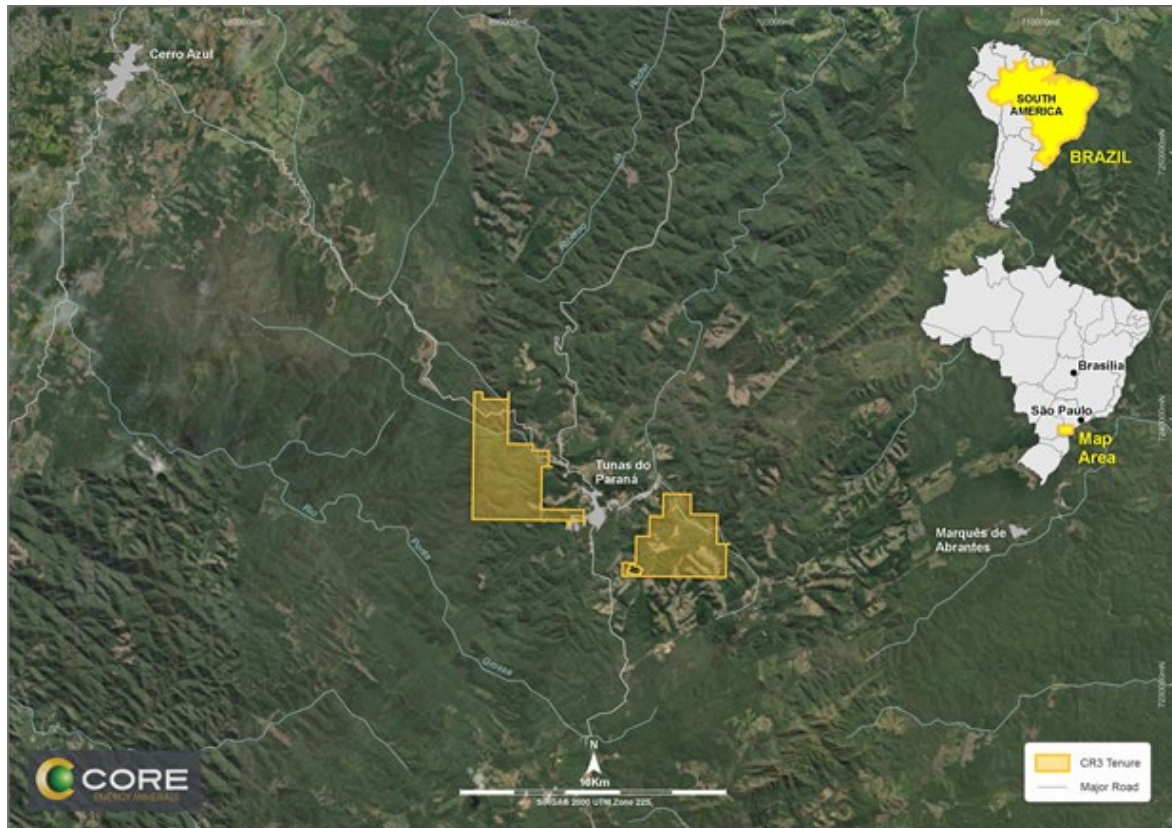


Figure 4: Tunas Project Exploration Licences location plan.

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This announcement has been authorised for release to ASX by the Board of Core Energy Minerals.

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About Core Energy Minerals Ltd

Core Energy Minerals Ltd (ASX:CR3) is a mineral exploration company with a critical minerals and uranium asset portfolio in tier one mining jurisdictions. Core Energy aims to advance its projects across Brazil and Australia, refining its focus, and unlocking shareholder value. Core Energy is currently focussed on its rare earth elements and uranium projects in Australia, Brazil and Namibia, with the Company exploring options to expand its land position in all jurisdictions.

Forward Looking Statement

This ASX announcement may include forward-looking statements. These forward-looking statements are not historical facts but rather are based on Core Energy Minerals Ltd's current expectations, estimates and assumptions about the industry in which Core Energy Minerals Ltd operates, and beliefs and assumptions regarding Core Energy Minerals Ltd's future performance. Words such as "anticipates", "expects", "intends", "plans", "believes", "seeks", "estimates", "potential" and similar expressions are intended to identify forward-

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Competent Person's Statement

The information relating to exploration results in this ASX Announcement for Core Energy Minerals Ltd was compiled by Mr Charles Nesbitt, a Competent Person, who is a member of the Australasian Institute of Mining and Metallurgy. Mr Nesbitt is an employee of Core Energy Minerals Ltd. Mr Nesbitt has sufficient experience, which is relevant to the style of mineralisation and types of deposits under consideration and to the activity to which he is undertaking to qualify as a "Competent Person" as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves.' Mr Nesbitt consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

All references to original source information are included as footnote and endnote references as indicated throughout the announcement where required.

APPENDIX 1 – Auger Hole locations

HoleID	X	Y	Z	Depth	Status
TNTR001	696433	7235678	892	10	Complete
TNTR002	696250	7235156	943	10	Complete
TNTR003	695583	7235619	976	10	Complete
TNTR004	696491	7236922	835	8.3	Complete
TNTR005	695857	7236002	846	9.55	Complete
TNTR006	695562	7235898	931	10	Complete
TNTR007	697577	7236274	909	8.5	Complete
TNTR008	696746	7236600	867	10	Complete
TNTR009	695906	7236473	873	10	Complete
TNTR010	697075	7236286	847	10	Complete
TNTR011	695986	7235519	805	4	Complete
TNTR012	695795	7235267	890	8	Complete
TNTR013	695286	7235230	961	0	Complete
TNTR014	696323	7235822	835	11	Complete
TNTR015	695949	7235963	916	1	Complete
TNTR016	696204	7235634	865	12.5	Complete
TNTR017	696009	7235278	860	10.3	Complete
TNTR018	697328	7236333	925	12.3	Complete
TNTR019	696117	7236224	901	12.5	Complete
TNTR020	696724	7236771	835	4	Complete
TNTR021	697746	7236126	904	2	Complete
TNTR022	697496	7236028	838	13.3	Complete
TNTR023	696772	7236972	873	14	Complete
TNTR024	695750	7235857	883	4.5	Complete
TNTR025	695754	7235862	884	5	Complete
TNTR026	696402	7235519	920	12.5	Complete
TNTR027	696252	7235388	884	12.5	Complete
TNTR028	695647	7235062	994	13	Complete
TNTR029	695425	7235045	954	10	Complete
TNTR030	695827	7235636	901	3	Complete
TNTR031	695828	7235642	896	2	Complete
TNTR032	695527	7235441	938	11	Complete

APPENDIX 2 – Leaching Results from Auger Holes

Auger Hole					Lab-Assay	Leaching Test Results							
HoleID	Sample ID	From (m)	To (m)	Interval (m)	TREO (ppm) ICP	TREO (ppm) Recovery	TREO Recovery	NdPr (ppm)	NdPr Recovery	DyTb (ppm)	DyTb (recovery)	Y2O3 (ppm)	Y2O3 recovery
TNTR014	SOCO0601	5	6	1.0	1125.2	715.8	64%	100.24	56%	346.21	79%	305.3	78%
TNTR014	SOCO0602	6	7	1.0	874.3	381.2	44%	54.83	42%	191.53	49%	169.8	54%
TNTR014	SOCO0603	7	8	1.0	514.2	206.9	40%	23.21	29%	118.82	51%	107.2	60%
TNTR014	SOCO0604	8	9	1.0	1457.7	125.8	9%	14.08	5%	67.74	12%	60.4	16%
TNTR014	SOCO0605	9	10	1.0	879.5	311.2	35%	40.49	26%	165.27	50%	146.8	57%
TNTR014	SOCO0606	10	11	1.0	1023.0	338.2	33%	44.03	25%	179.02	44%	159.4	52%
TNTR016	SOCO0612	4	5	1.0	829.5	33.8	4%	11.85	27%	3.28	7%	3.1	8%
TNTR016	SOCO0613	5	6	1.0	1245.9	37.4	3%	12.56	14%	1.30	5%	1.2	2%
TNTR016	SOCO0614	6	7	1.0	1799.6	35.2	2%	13.15	6%	1.14	3%	1.0	1%
TNTR016	SOCO0615	7	8	1.0	1823.3	33.7	2%	13.14	4%	1.20	2%	1.0	1%
TNTR016	SOCO0616	8	9	1.0	2109.2	38.4	2%	14.47	5%	1.42	3%	1.0	1%
TNTR016	SOCO0617	9	10	1.0	2077.9	41.2	2%	15.15	5%	1.88	5%	1.3	1%
TNTR016	SOCO0618	10	11	1.0	1506.5	33.0	2%	13.99	6%	1.34	4%	1.0	1%
TNTR016	SOCO0619	11	12	1.0	1241.4	68.8	6%	26.12	11%	5.36	10%	4.1	6%
TNTR016	SOCO0620	12	12.5	0.5	1385.5	128.7	9%	46.48	16%	19.65	16%	17.0	20%
TNTR017	SOCO0628	7	8	1.0	970.3	47.7	5%	13.02	7%	1.20	4%	1.0	3%
TNTR017	SOCO0629	8	9	1.0	2647.0	55.7	2%	13.13	2%	2.18	2%	1.7	2%
TNTR017	SOCO0630	9	10.3	1.3	2957.4	95.1	3%	20.61	3%	10.54	4%	8.4	5%
TNTR018	SOCO0631	0	1	1.0	1409.4	49.6	4%	12.62	12%	1.14	6%	1.0	4%
TNTR018	SOCO0632	1	2	1.0	1238.3	46.5	4%	12.70	14%	1.14	7%	1.0	4%
TNTR018	SOCO0633	2	3	1.0	655.0	37.1	6%	12.61	18%	1.14	11%	1.0	6%
TNTR018	SOCO0634	3	4	1.0	1241.3	95.7	8%	40.31	27%	1.57	13%	1.0	4%
TNTR018	SOCO0635	4	5	1.0	1059.3	387.1	37%	209.25	60%	12.54	39%	9.1	25%
TNTR018	SOCO0636	5	6	1.0	1878.3	514.0	27%	306.19	45%	15.32	26%	11.4	18%
TNTR018	SOCO0637	6	7	1.0	2603.6	717.5	28%	416.48	40%	20.07	23%	15.0	16%
TNTR018	SOCO0638	7	8	1.0	2804.6	1139.8	41%	610.74	57%	43.24	37%	33.9	31%
TNTR018	SOCO0639	8	9	1.0	2437.0	1097.8	45%	515.35	60%	60.05	52%	47.9	48%
TNTR018	SOCO0640	9	10	1.0	2802.0	506.1	18%	209.33	26%	38.09	24%	30.5	22%
TNTR018	SOCO0641	10	11	1.0	2944.9	1419.6	48%	515.16	61%	165.16	61%	136.3	61%
TNTR018	SOCO0642	11	12.3	1.3	2853.5	1822.6	64%	592.76	80%	288.99	86%	242.1	90%

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APPENDIX 3 – Mechanized Auger Hole Assay TREO results (sieved sampling method)

Hole_ID	SampleID	Depth From	Depth To	CeO2 ppm	Dy2O3 ppm	Er2O3 ppm	Eu2O3 ppm	Gd2O3 ppm	Ho2O3 ppm	La2O3 ppm	Lu2O3 ppm	Nd2O3 ppm	Pr6O11 ppm	Sm2O3 ppm	Tb4O7 ppm	Tm2O3 ppm	Y2O3 ppm	Yb2O3 ppm	TREO ppm	HREO (%)	MREO (%)	NdPr (ppm)	DyTb (ppm)
TNTR025	SOCO0712	0	1	344.0	5.1	3.4	0.9	4.3	1.0	48.2	0.5	24.6	8.1	4.6	0.7	0.5	28.5	3.9	478.2	11%	8%	32.7	5.8
TNTR025	SOCO0714	1	2	280.6	5.2	3.8	0.9	3.9	1.1	41.0	0.6	21.0	7.1	4.5	0.7	0.6	32.4	4.2	407.6	14%	8%	28.1	5.9
TNTR025	SOCO0716	2	3	219.9	10.2	5.9	1.5	8.8	1.9	68.3	0.7	44.0	13.7	8.8	1.4	0.8	56.8	5.7	448.1	23%	15%	57.7	11.6
TNTR025	SOCO0718	3	4	215.5	8.1	4.6	1.5	8.2	1.5	76.6	0.6	51.2	15.6	10.0	1.3	0.6	42.8	4.4	442.4	19%	17%	66.8	9.4
TNTR025	SOCO0720	4	5	234.5	7.7	4.8	1.5	7.4	1.5	81.5	0.7	51.4	16.0	9.3	1.2	0.7	43.8	4.8	466.7	18%	16%	67.4	8.8
TNTR026	SOCO0722	0	1	119.2	5.5	3.0	1.5	6.1	1.0	56.2	0.4	39.8	11.7	7.0	0.9	0.4	26.7	3.0	282.3	20%	21%	51.5	6.4
TNTR026	SOCO0724	1	2	156.1	6.4	3.0	1.9	7.2	1.0	68.7	0.4	46.4	14.7	9.5	1.0	0.4	26.0	2.8	345.6	17%	20%	61.1	7.5
TNTR026	SOCO0726	2	3	221.8	8.3	4.0	2.7	9.9	1.5	99.5	0.4	77.7	23.6	12.6	1.5	0.5	37.6	3.2	504.9	16%	22%	101.3	9.8
TNTR026	SOCO0728	3	4	294.4	10.2	4.4	3.1	11.6	1.7	116.0	0.4	78.1	24.1	15.7	1.6	0.5	38.8	3.5	604.2	15%	19%	102.2	11.9
TNTR026	SOCO0730	4	5	302.7	7.8	3.8	2.1	8.8	1.3	74.7	0.4	49.8	15.7	10.7	1.2	0.4	28.7	3.0	510.9	13%	15%	65.5	9.0
TNTR026	SOCO0732	5	6	116.2	5.8	3.6	1.3	5.2	1.1	30.1	0.6	22.9	6.7	5.3	0.8	0.5	23.7	4.3	228.1	23%	16%	29.6	6.6
TNTR026	SOCO0734	6	7	400.8	14.0	5.2	4.8	19.3	1.9	189.1	0.4	133.0	41.3	25.4	2.5	0.6	47.1	4.0	889.5	14%	21%	174.3	16.5
TNTR026	SOCO0736	7	8	419.3	15.2	5.7	5.0	20.0	2.4	200.1	0.5	143.1	43.7	26.9	2.6	0.6	54.2	4.0	943.2	15%	22%	186.8	17.8
TNTR026	SOCO0738	8	9	369.4	6.8	3.0	2.0	8.0	1.1	89.1	0.4	57.7	17.9	10.3	1.1	0.4	25.3	2.7	595.2	10%	14%	75.6	7.8
TNTR026	SOCO0740	9	10	228.5	4.2	2.3	1.1	4.2	0.7	40.2	0.4	26.6	8.5	5.1	0.7	0.3	13.9	2.7	339.5	11%	12%	35.1	4.8
TNTR026	SOCO0742	10	11	234.9	4.2	2.3	1.0	3.9	0.7	37.1	0.4	26.8	8.1	5.8	0.6	0.4	14.6	2.7	343.5	11%	12%	35.0	4.8
TNTR026	SOCO0744	11	12	139.4	7.5	2.9	2.6	8.8	1.1	78.7	0.4	56.3	17.0	11.5	1.2	0.4	23.3	2.6	353.7	18%	23%	73.4	8.7
TNTR026	SOCO0746	12	12.5	206.7	7.6	3.1	2.5	9.3	1.2	81.2	0.4	57.5	17.3	11.7	1.2	0.4	24.6	3.0	427.6	15%	20%	74.8	8.8
TNTR027	SOCO0748	0	1	192.6	7.2	3.5	1.9	8.5	1.2	77.8	0.4	55.3	16.8	10.9	1.2	0.4	30.8	3.3	411.7	17%	20%	72.1	8.4
TNTR027	SOCO0750	1	2	188.6	6.5	3.5	1.9	7.4	1.1	66.6	0.4	48.1	14.3	9.5	1.0	0.4	29.2	3.3	381.9	17%	18%	62.4	7.6
TNTR027	SOCO0852	2	3	268.0	6.4	3.0	1.8	7.4	1.1	89.1	0.3	56.2	18.1	10.6	1.1	0.4	25.4	2.7	491.5	12%	17%	74.3	7.4
TNTR027	SOCO0854	3	4	209.7	6.2	2.9	1.6	6.9	1.1	90.0	0.3	51.8	17.0	9.5	1.0	0.4	23.6	2.8	424.8	13%	18%	68.8	7.2
TNTR027	SOCO0856	4	5	226.3	6.8	3.1	1.9	8.5	1.1	107.7	0.3	64.3	21.2	12.3	1.2	0.4	26.0	2.6	483.5	13%	19%	85.4	7.9
TNTR027	SOCO0858	5	6	275.3	8.7	3.9	2.6	11.4	1.5	138.6	0.4	88.8	29.1	15.1	1.5	0.5	35.4	3.1	615.8	14%	21%	117.9	10.3
TNTR027	SOCO0860	6	7	227.4	9.7	4.6	2.8	12.6	1.6	133.2	0.4	87.1	27.6	16.2	1.7	0.5	40.6	3.4	569.4	17%	22%	114.7	11.4

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Hole_ID	SampleID	Depth From	Depth To	CeO2 ppm	Dy2O3 ppm	Er2O3 ppm	Eu2O3 ppm	Gd2O3 ppm	Ho2O3 ppm	La2O3 ppm	Lu2O3 ppm	Nd2O3 ppm	Pr6O11 ppm	Sm2O3 ppm	Tb4O7 ppm	Tm2O3 ppm	Y2O3 ppm	Yb2O3 ppm	TREO ppm	HREO (%)	MREO (%)	NdPr (ppm)	DyTb (ppm)
TNTR027	SOCO0862	7	8	186.6	10.6	4.4	2.9	13.3	1.7	130.2	0.4	90.3	27.6	16.9	1.8	0.5	40.6	3.5	531.4	18%	25%	117.9	12.4
TNTR027	SOCO0864	8	9	153.1	8.5	3.5	2.4	11.0	1.4	107.4	0.4	73.8	22.6	14.0	1.5	0.4	34.1	3.1	437.4	18%	24%	96.5	10.1
TNTR027	SOCO0866	9	10	222.7	6.1	3.2	1.6	7.0	1.0	69.5	0.4	50.2	15.3	9.4	0.9	0.4	24.6	3.0	415.2	14%	17%	65.4	7.0
TNTR027	SOCO0868	10	11	172.7	6.3	3.0	2.0	8.0	1.0	77.9	0.4	65.3	18.6	11.4	1.0	0.4	24.6	3.0	395.5	15%	23%	83.9	7.3
TNTR027	SOCO0870	11	12	96.6	7.2	3.8	2.7	9.4	1.2	89.1	0.7	101.1	26.0	17.4	1.1	0.6	31.1	4.2	392.3	20%	35%	127.2	8.3
TNTR027	SOCO0872	12	12.5	230.3	6.3	3.0	1.8	7.5	1.1	78.5	0.4	60.0	17.7	10.3	1.0	0.4	25.0	2.8	446.1	13%	19%	77.7	7.3
TNTR028	SOCO0874	0	1	188.3	3.8	2.8	0.6	3.0	0.8	30.8	0.5	15.6	5.2	3.5	0.5	0.4	20.1	3.3	279.3	14%	9%	20.8	4.3
TNTR028	SOCO0876	1	2	334.1	3.3	2.3	0.4	2.1	0.7	23.0	0.6	11.0	3.7	2.4	0.4	0.4	17.7	3.2	405.4	8%	5%	14.6	3.8
TNTR028	SOCO0878	2	3	169.8	4.1	1.9	0.9	3.1	0.7	9.0	0.3	9.6	2.6	3.4	0.6	0.3	14.5	2.0	222.7	14%	8%	12.2	4.7
TNTR028	SOCO0880	3	4	113.1	3.5	1.9	1.0	3.2	0.6	8.0	0.3	9.2	2.6	3.0	0.5	0.3	13.5	2.2	163.0	18%	10%	11.8	4.0
TNTR028	SOCO0882	4	5	484.1	4.6	2.8	1.1	3.7	0.9	8.4	0.4	10.7	2.8	3.8	0.7	0.4	18.5	3.0	545.9	7%	3%	13.5	5.3
TNTR028	SOCO0884	5	6	179.3	5.2	3.3	1.2	4.3	1.0	13.1	0.4	16.1	4.1	4.1	0.7	0.5	20.7	3.6	257.8	17%	10%	20.2	6.0
TNTR028	SOCO0886	6	7	89.4	5.7	3.7	1.4	4.9	1.0	17.9	0.5	18.7	5.1	5.7	0.8	0.5	23.7	4.0	183.1	28%	17%	23.8	6.6
TNTR028	SOCO0888	7	8	66.8	6.8	4.3	1.7	5.6	1.2	18.8	0.6	17.4	4.6	5.7	0.9	0.6	26.0	4.2	165.0	35%	18%	22.0	7.7
TNTR028	SOCO0890	8	9	70.8	6.4	4.2	1.5	6.0	1.2	18.9	0.6	17.5	4.5	5.1	1.0	0.6	26.8	4.4	169.5	34%	17%	22.0	7.4
TNTR028	SOCO0892	9	10	128.9	5.9	3.9	1.4	4.9	1.1	16.1	0.5	32.7	11.0	4.4	0.9	0.5	26.7	4.1	242.8	22%	21%	43.6	6.8
TNTR028	SOCO0894	10	11	207.6	5.5	3.5	1.2	4.2	1.0	17.7	0.5	13.8	4.1	3.8	0.7	0.5	23.3	3.5	290.9	16%	8%	17.9	6.2
TNTR028	SOCO0896	11	12	166.1	4.4	3.1	1.1	3.9	0.9	12.2	0.4	12.2	3.4	3.9	0.7	0.4	19.5	3.1	235.2	18%	9%	15.6	5.1
TNTR028	SOCO0898	12	13	98.1	4.9	3.1	1.1	4.0	0.9	14.2	0.5	15.5	4.2	4.6	0.7	0.4	20.8	3.4	176.7	25%	14%	19.7	5.6
TNTR029	SOCO0900	0	1	887.9	6.1	4.0	1.0	5.1	1.1	51.1	0.5	29.9	9.7	5.9	0.9	0.5	33.7	4.3	1,041.8	6%	4%	39.5	7.0
TNTR029	SOCO0902	1	2	864.3	7.2	5.0	1.0	5.6	1.4	51.0	0.7	34.1	10.6	6.0	0.9	0.7	39.4	5.4	1,033.4	7%	5%	44.7	8.2
TNTR029	SOCO0904	2	3	536.0	8.4	5.5	1.4	6.4	1.6	65.9	0.7	49.5	14.8	9.3	1.1	0.8	46.1	5.6	753.0	12%	10%	64.2	9.5
TNTR029	SOCO0906	3	4	273.0	10.5	6.2	3.0	13.0	1.9	142.3	0.8	114.4	35.0	20.5	1.7	0.9	53.5	6.4	682.9	17%	24%	149.4	12.2
TNTR029	SOCO0908	4	5	485.6	77.5	36.1	18.4	100.1	12.5	714.1	3.8	512.2	148.5	107.7	13.4	4.4	332.8	30.7	2,598.0	28%	29%	660.7	91.0
TNTR029	SOCO0910	5	6	326.4	89.1	41.4	21.2	116.0	14.7	885.2	4.2	616.8	180.9	128.8	15.1	5.2	417.9	34.6	2,897.5	31%	31%	797.7	104.1
TNTR029	SOCO0912	6	7	587.7	31.3	16.0	7.7	40.6	5.7	380.3	1.9	297.0	87.3	53.3	5.5	2.3	166.5	14.6	1,697.6	20%	25%	384.3	36.8
TNTR029	SOCO0914	7	8	1,167.7	32.6	16.3	8.7	44.5	5.9	409.8	2.0	359.4	104.9	61.9	5.9	2.2	160.6	14.6	2,396.9	15%	21%	464.3	38.6
TNTR029	SOCO0916	8	9	800.8	42.8	21.2	11.4	57.6	7.6	495.7	2.5	423.1	123.8	78.2	7.7	2.8	214.3	18.6	2,307.9	20%	26%	546.8	50.5

ASX Announcement

Hole_ID	SampleID	Depth From	Depth To	CeO2 ppm	Dy2O3 ppm	Er2O3 ppm	Eu2O3 ppm	Gd2O3 ppm	Ho2O3 ppm	La2O3 ppm	Lu2O3 ppm	Nd2O3 ppm	Pr6O11 ppm	Sm2O3 ppm	Tb4O7 ppm	Tm2O3 ppm	Y2O3 ppm	Yb2O3 ppm	TREO ppm	HREO (%)	MREO (%)	NdPr (ppm)	DyTb (ppm)
TNTR029	SOCO0918	9	10	816.9	48.3	24.6	12.4	64.3	8.6	518.8	3.0	487.6	141.9	81.8	8.8	3.3	251.6	21.3	2,493.2	21%	28%	629.4	57.1
TNTR030	SOCO0920	0	1	195.8	6.7	3.1	1.8	7.5	1.2	71.7	0.4	57.3	17.7	10.3	1.1	0.5	27.7	3.1	406.0	16%	20%	74.9	7.9
TNTR030	SOCO0922	1	2	306.6	6.3	3.2	1.8	7.8	1.1	74.5	0.4	66.4	20.6	9.9	1.1	0.4	26.2	2.7	529.0	12%	18%	87.0	7.4
TNTR030	SOCO0924	2	3	392.1	7.4	3.2	2.6	10.1	1.3	101.1	0.4	76.9	23.0	13.6	1.4	0.4	24.7	2.8	661.0	10%	16%	99.9	8.8
TNTR031	SOCO0926	0	1	156.0	5.6	3.0	1.5	6.7	1.0	58.1	0.4	40.8	12.1	7.4	0.9	0.4	23.2	2.8	319.9	17%	19%	52.9	6.5
TNTR031	SOCO0928	1	2	158.0	5.8	2.9	1.7	6.7	1.0	63.6	0.4	49.7	15.4	8.2	1.0	0.4	24.5	3.0	342.2	16%	21%	65.0	6.8
TNTR032	SOCO0930	0	1	199.2	2.7	1.8	0.3	1.8	0.5	26.4	0.3	11.3	4.2	2.2	0.3	0.3	12.9	2.4	266.5	10%	7%	15.5	3.0
TNTR032	SOCO0932	1	2	160.1	1.4	1.4	0.1	0.9	0.4	11.1	0.3	4.5	1.7	0.9	0.2	0.3	6.7	2.0	192.0	8%	4%	6.3	1.5
TNTR032	SOCO0934	2	3	282.2	1.8	1.4	0.2	1.3	0.4	23.7	0.3	6.1	2.5	1.3	0.3	0.2	8.4	1.8	331.8	5%	3%	8.5	2.1
TNTR032	SOCO0936	3	4	840.2	2.2	2.0	0.2	1.4	0.5	12.5	0.4	7.2	2.4	1.6	0.3	0.4	10.3	2.7	884.4	2%	1%	9.6	2.5
TNTR032	SOCO0938	4	5	919.8	2.3	1.5	0.4	1.9	0.4	18.4	0.3	15.6	5.0	2.9	0.3	0.2	8.9	2.0	980.0	2%	2%	20.6	2.6
TNTR032	SOCO0940	5	6	977.1	3.1	2.1	0.5	3.4	0.7	41.3	0.4	27.8	9.3	4.6	0.5	0.3	14.3	2.6	1,087.9	3%	4%	37.0	3.6
TNTR032	SOCO0942	6	7	1,201.7	7.5	4.6	0.9	7.5	1.4	80.5	0.7	50.0	15.9	9.6	1.2	0.7	37.9	4.7	1,424.7	5%	5%	66.0	8.6
TNTR032	SOCO0944	7	8	865.3	8.4	4.7	1.1	8.5	1.5	82.1	0.7	59.4	18.3	10.4	1.3	0.7	39.1	5.2	1,106.6	7%	8%	77.6	9.7
TNTR032	SOCO0946	8	9	794.9	9.9	5.2	1.1	9.9	1.8	127.8	0.7	71.5	23.6	12.6	1.5	0.7	47.8	5.1	1,114.3	9%	10%	95.1	11.4
TNTR032	SOCO0948	9	10	557.8	22.0	11.0	3.4	24.3	3.8	207.1	1.4	178.3	57.7	33.7	3.8	1.6	93.4	11.2	1,210.7	17%	22%	236.0	25.9
TNTR032	SOCO0950	10	11	690.0	38.4	18.2	5.1	40.7	6.3	276.0	2.2	233.3	76.1	48.8	6.5	2.6	166.2	17.9	1,628.2	22%	22%	309.3	44.8

APPENDIX 4 - JORC Code, 2012 Edition – Table 1
Section 1: Sampling Techniques and Data

Criteria	Explanation	Comment
Sampling techniques	<i>Nature and quality of sampling (e.g., cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g., 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg., submarine nodules) may warrant disclosure of detailed information.</i>	- Samples were collected at 1m intervals throughout the auger drilling program, with the exception of the final sample of the drill hole where the hole did not reach a whole metre. - Material recovered from each interval was placed on a plastic tarpaulin and manually homogenised by lifting and mixing the sample using the tarpaulin edges to ensure representative sample distribution. - A standard cone-and-quartering method was applied in the field, with approximately one quarter of the homogenised material (typically 2–3kg) retained as the primary sample for analysis. - To minimise the potential for contamination between intervals, the first approximately 5cm of recovered material from each sample interval was discarded prior to sample collection. - From auger holes TNTR025 to TNTR032, duplicate sample preparation protocols were implemented. Following homogenisation and cone-and-quartering, two sub-samples were collected from each 1m interval: (i) a bulk (unsieved) sample and (ii) a sample sieved to <2mm (10# mesh) in the field and subsequently screened to <80# mesh in the laboratory. Both sample types were submitted for analysis to evaluate the influence of particle-size fractions on assay results. - All samples were geologically logged and recorded in a digital database, with representative photographs collected for documentation and verification purposes. - Samples were placed in sealed plastic bags, double-bagged for security, labelled with uniquely numbered sample tags and dispatched to SGS Geosol laboratory in Vespasiano-MG under standard chain-of-custody procedures for geochemical analysis.
Drilling techniques	<i>Drill type (e.g., core, reverse circulation, open- hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g., core diameter, triple or standard tube, depth of diamond tails, face-sampling bit, or other type, whether core is oriented and if so, by what method, etc).</i>	- The auger-drilling was completed in-house by the CR3 team using a powered mechanised auger equipment during March to April 2026. - A total of 19 auger holes were completed for 166.40 metres of drilling. - All drill holes were drilled vertically using auger flights of approximately 100 mm diameter. - Drill hole locations were planned on an approximate 200m × 300m spacing, with local variations reflecting access, topography and geological considerations. - Drilling was designed to test the lateral continuity and vertical distribution of REE mineralisation within the weathered regolith profile developed over biotite gneiss.

Criteria	Explanation	Comment
<i>Drill sample recovery</i>	<i>Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples.</i>	- Auger samples are laid out in meter intervals, visual estimate of recovery is made. All holes/spoil are photographed. - No significant sampling issue were noted, recovery issue or bias was picked up and it is therefore considered that both sample recovery and quality is adequate for the drilling technique employed.
	<i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i>	No known sample bias due to recovery has occurred.
<i>Logging</i>	<i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i> <i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i> <i>The total length and percentage of the relevant intersections logged.</i>	- Geological logging is qualitative in nature. - Auger samples are laid out in meter intervals for visual logging and determination of select intervals to be sampled at targeted horizons and all material recovered are photographed and qualitatively logged for visual characteristics, such as composition and percentage of clay and oxides.
<i>Sub-sampling techniques and sample preparation</i>	<i>If core, whether cut or sawn and whether quarter, half or all cores taken.</i> <i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i> <i>For all sample types, the nature, quality, and appropriateness of the sample preparation technique.</i> <i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i> <i>Measures taken to ensure that the sampling is representative of the in- situ material collected, including for instance results for field duplicate/second-half sampling.</i> <i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i>	- Auger samples were collected over targeted 1 m intervals. Material from each interval was coned and quartered in the field to obtain a representative sub-sample of approximately 2–3 kg. - Samples were photographed in the field, labelled with unique identifiers, and prepared for dispatch to the laboratory. - All laboratory sample preparation was undertaken by SGS Geosol. - For the auger holes TNTR025 to TNTR032, duplicate sample preparation protocols were implemented for comparison purposes. For each 1 m interval, two sub-samples were prepared: (i) a sample sieved to 10# mesh in the field and subsequently screened to 80# in the laboratory, and (ii) a bulk sample submitted without prior sieving and fully prepared in the laboratory. - The auger program is considered early-stage exploration. No field duplicates, certified reference materials (standards), or blanks were included in the sampling program. - Selected auger samples were submitted for leach test work based on prior ICP assay results, geological logging and their position within the weathered profile. Samples were selected to test the leachability of mineralised intervals considered representative of clay-rich weathered material at the Tunas Project (appendix 2).

Criteria	Explanation	Comment																																																																						
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (e.g., standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e., lack of bias) and precision have been established.	- Samples were analysed at SGS-Geosol laboratory, located in Vespasiano, MG, Brazil. The laboratory is certified ISO9001:2015, ISO14001:2015 and ISO17025:2017. - Sample preparation comprises an industry standard of drying the material, crushing 75% at 3mm size, homogeneizing with a Jones Splitter and pulverising between 250 and 300g (95% at 150#). - The analytical methodologies used are identified by the codes ICP95A (ICP-OES), which comprises 11 oxides and 5 elements and IMS95A (ICP-MS), which comprises 30 elements, both determined by lithium metaborate fusion. - For fusion with lithium metaborate, graphite crucibles are used, in which initially 0.5 g of lithium metaborate, 0.1 g of pulverised sample and other 0.5 g of lithium metaborate are inserted. Heated up to 950°C. Molten content is placed in beaker with 100ml solution of 2% tartaric acid (C4H6O6), 10% nitric acid (HNO3) and 88% purified water for homogenization. Two aliquots with 15ml each are transferred to test tubes and are sent for ICP analysis (analytical reference IMS95A). - The analyses are performed through mass spectrometry with inductively coupled plasma (ICP-MS). In this procedure, the ions are separated according to the mass / charge ratio through transport under the action of electric and magnetic fields. Quantitative analyses include 15 rare earth elements, in addition to Y, Co, Cu, Cs, Ga, Hf, Mo, Ni, Rb, Sn, Ta, Th, Tl, U and W (ICP-MS-IMS-95A). Detection limits are shown in the Table below. <table><tr><th colspan="4">Determinação por Fusão com Metaborato de Lítio - ICP OES</th><th>PM-000003/3</th></tr><tr><td>Al2O3 0.01 - 75 (%)</td><td>Ba 10 - 100000 (ppm)</td><td>CaO 0.01 - 60 (%)</td><td>Cr2O3 0.01 - 10 (%)</td><td></td></tr><tr><td>Fe2O3 0.01 - 75 (%)</td><td>K2O 0.01 - 25 (%)</td><td>MgO 0.01 - 30 (%)</td><td>MnO 0.01 - 10 (%)</td><td></td></tr><tr><td>Na2O 0.01 - 30 (%)</td><td>P2O5 0.01 - 25 (%)</td><td>SiO2 0.01 - 90 (%)</td><td>Sr 10 - 100000 (ppm)</td><td></td></tr><tr><td>TiO2 0.01 - 25 (%)</td><td>V 5 - 10000 (ppm)</td><td>Zn 5 - 10000 (ppm)</td><td>Zr 10 - 100000 (ppm)</td><td></td></tr></table> <table><tr><th colspan="4">Determinação por Fusão com Metaborato de Lítio - ICP MS</th><th>PM-000003/3</th></tr><tr><td>Ce 0.1 - 10000 (ppm)</td><td>Co 0.5 - 10000 (ppm)</td><td>Cs 0.05 - 1000 (ppm)</td><td>Cu 5 - 10000 (ppm)</td><td></td></tr><tr><td>Dy 0.05 - 1000 (ppm)</td><td>Er 0.05 - 1000 (ppm)</td><td>Eu 0.05 - 1000 (ppm)</td><td>Ga 0.1 - 10000 (ppm)</td><td></td></tr><tr><td>Gd 0.05 - 1000 (ppm)</td><td>Hf 0.05 - 500 (ppm)</td><td>Ho 0.05 - 1000 (ppm)</td><td>La 0.1 - 10000 (ppm)</td><td></td></tr><tr><td>Lu 0.05 - 1000 (ppm)</td><td>Mo 2 - 10000 (ppm)</td><td>Nb 0.05 - 1000 (ppm)</td><td>Nd 0.1 - 10000 (ppm)</td><td></td></tr><tr><td>Ni 5 - 10000 (ppm)</td><td>Pr 0.05 - 1000 (ppm)</td><td>Rb 0.2 - 10000 (ppm)</td><td>Sm 0.1 - 1000 (ppm)</td><td></td></tr><tr><td>Sn 0.3 - 1000 (ppm)</td><td>Ta 0.05 - 10000 (ppm)</td><td>Tb 0.05 - 1000 (ppm)</td><td>Th 0.1 - 10000 (ppm)</td><td></td></tr><tr><td>Tl 0.5 - 1000 (ppm)</td><td>Tm 0.05 - 1000 (ppm)</td><td>U 0.05 - 10000 (ppm)</td><td>W 0.1 - 10000 (ppm)</td><td></td></tr><tr><td>Y 0.05 - 10000 (ppm)</td><td>Yb 0.1 - 1000 (ppm)</td><td></td><td></td><td></td></tr></table> - No standard, duplicate, or blank control samples were inserted by the Company during this early-stage exploration phase. The Company acknowledges the absence of QA/QC protocols in this stage and notes that appropriate quality control procedures will be implemented in subsequent phases of the program. Results in this document are reported as rare earth oxides (REO), in accordance with industry-standard practices. The total rare earth oxide content (TREO) is calculated as the sum of individual 15 REOs. The following calculations are used for compiling REO into their reporting and evaluation groups: - TREO (Total Rare Earth Oxide) = [La2O3] + [CeO2] + [Pr6O11] + [Nd2O3] + [Sm2O3] + [Eu2O3] + [Gd2O3] + [Tb4O7] + [Dy2O3] + [Ho2O3] + [Er2O3] + [Tm2O3] + [Yb2O3] + [Y2O3] + [Lu2O3]. - LREO (Light Rare Earth Oxide) = [CeO2] + [La2O3] + [Nd2O3] + [Pr6O11] - HREO (Heavy Rare Earth Oxide) = [Eu2O3] + [Gd2O3] + [Tb4O7] + [Dy2O3] + [Ho2O3] + [Er2O3] + [Tm2O3] + [Yb2O3] + [Y2O3] +	Determinação por Fusão com Metaborato de Lítio - ICP OES				PM-000003/3	Al2O3 0.01 - 75 (%)	Ba 10 - 100000 (ppm)	CaO 0.01 - 60 (%)	Cr2O3 0.01 - 10 (%)		Fe2O3 0.01 - 75 (%)	K2O 0.01 - 25 (%)	MgO 0.01 - 30 (%)	MnO 0.01 - 10 (%)		Na2O 0.01 - 30 (%)	P2O5 0.01 - 25 (%)	SiO2 0.01 - 90 (%)	Sr 10 - 100000 (ppm)		TiO2 0.01 - 25 (%)	V 5 - 10000 (ppm)	Zn 5 - 10000 (ppm)	Zr 10 - 100000 (ppm)		Determinação por Fusão com Metaborato de Lítio - ICP MS				PM-000003/3	Ce 0.1 - 10000 (ppm)	Co 0.5 - 10000 (ppm)	Cs 0.05 - 1000 (ppm)	Cu 5 - 10000 (ppm)		Dy 0.05 - 1000 (ppm)	Er 0.05 - 1000 (ppm)	Eu 0.05 - 1000 (ppm)	Ga 0.1 - 10000 (ppm)		Gd 0.05 - 1000 (ppm)	Hf 0.05 - 500 (ppm)	Ho 0.05 - 1000 (ppm)	La 0.1 - 10000 (ppm)		Lu 0.05 - 1000 (ppm)	Mo 2 - 10000 (ppm)	Nb 0.05 - 1000 (ppm)	Nd 0.1 - 10000 (ppm)		Ni 5 - 10000 (ppm)	Pr 0.05 - 1000 (ppm)	Rb 0.2 - 10000 (ppm)	Sm 0.1 - 1000 (ppm)		Sn 0.3 - 1000 (ppm)	Ta 0.05 - 10000 (ppm)	Tb 0.05 - 1000 (ppm)	Th 0.1 - 10000 (ppm)		Tl 0.5 - 1000 (ppm)	Tm 0.05 - 1000 (ppm)	U 0.05 - 10000 (ppm)	W 0.1 - 10000 (ppm)		Y 0.05 - 10000 (ppm)	Yb 0.1 - 1000 (ppm)			
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Lu 0.05 - 1000 (ppm)	Mo 2 - 10000 (ppm)	Nb 0.05 - 1000 (ppm)	Nd 0.1 - 10000 (ppm)																																																																					
Ni 5 - 10000 (ppm)	Pr 0.05 - 1000 (ppm)	Rb 0.2 - 10000 (ppm)	Sm 0.1 - 1000 (ppm)																																																																					
Sn 0.3 - 1000 (ppm)	Ta 0.05 - 10000 (ppm)	Tb 0.05 - 1000 (ppm)	Th 0.1 - 10000 (ppm)																																																																					
Tl 0.5 - 1000 (ppm)	Tm 0.05 - 1000 (ppm)	U 0.05 - 10000 (ppm)	W 0.1 - 10000 (ppm)																																																																					
Y 0.05 - 10000 (ppm)	Yb 0.1 - 1000 (ppm)																																																																							

Criteria	Explanation	Comment																																																
		[Lu2O3] - CREO (Critical Rare Earth Oxide) = [Nd2O3] + [Eu2O3] + [Tb4O7] + [Dy2O3] + [Y2O3] - MREO (Magnetic Rare Earth Oxide) = [Pr6O11] + [Nd2O3] + [Tb4O7] + [Dy2O3] - Y2O3 has been reported separately due to its current economic and strategic value. Y2O3 also remains included within TREO, CREO and HREO calculations unless otherwise stated. - All results of this report are presented in ppm and the REE elements were converted to their stoichiometric oxide forms using standard conversion factors from Advanced Analytical Centre, James Cook University. The conversion factors are shown in the table below. <table border="1"> <thead> <tr> <th>TREO</th><th>REE Oxides</th><th>Conversion factor (Element → Oxide)</th></tr> </thead> <tbody> <tr><td>Cério (Ce)</td><td>CeO₂</td><td>1.2284</td></tr> <tr><td>Disprósio (Dy)</td><td>Dy₂O₃</td><td>1.1477</td></tr> <tr><td>Érbio (Er)</td><td>Er₂O₃</td><td>1.1435</td></tr> <tr><td>Európio (Eu)</td><td>Eu₂O₃</td><td>1.1579</td></tr> <tr><td>Gadolinio (Gd)</td><td>Gd₂O₃</td><td>1.1526</td></tr> <tr><td>Hólmio (Ho)</td><td>Ho₂O₃</td><td>1.1455</td></tr> <tr><td>Íterbio (Yb)</td><td>Yb₂O₃</td><td>1.1387</td></tr> <tr><td>Ítrio (Y)</td><td>Y₂O₃</td><td>1.2699</td></tr> <tr><td>Lantânio (La)</td><td>La₂O₃</td><td>1.1728</td></tr> <tr><td>Lutécio (Lu)</td><td>Lu₂O₃</td><td>1.1371</td></tr> <tr><td>Neodímio (Nd)</td><td>Nd₂O₃</td><td>1.1664</td></tr> <tr><td>Praseodímio (Pr)</td><td>Pr₆O₁₁</td><td>1.2082</td></tr> <tr><td>Samário (Sm)</td><td>Sm₂O₃</td><td>1.1596</td></tr> <tr><td>Térbio (Tb)</td><td>Tb₄O₇</td><td>1.1762</td></tr> <tr><td>Túlio (Tm)</td><td>Tm₂O₃</td><td>1.1421</td></tr> </tbody> </table> - The adopted QA/QC protocols are appropriate for this stage of test work. The sample preparation and assay techniques to be used are industry standard and provide a total analysis. - Leach test work was completed by SGS Geosol to assess the recoverability of rare earth mineralisation under mild leaching conditions. Testing was undertaken using a 0.5 molar ammonium sulphate solution as the lixiviant, with a 30-minute leach duration. The initial pH was adjusted to 4, with pH control applied only at the start of dissolution. - Leach solutions were analysed by ICP-OES and ICP-MS. Recoveries were calculated by comparing the rare earth element values recovered in the leach solution against the corresponding rare earth element values of the original sample as determined by ICP analysis.	TREO	REE Oxides	Conversion factor (Element → Oxide)	Cério (Ce)	CeO ₂	1.2284	Disprósio (Dy)	Dy ₂ O ₃	1.1477	Érbio (Er)	Er ₂ O ₃	1.1435	Európio (Eu)	Eu ₂ O ₃	1.1579	Gadolinio (Gd)	Gd ₂ O ₃	1.1526	Hólmio (Ho)	Ho ₂ O ₃	1.1455	Íterbio (Yb)	Yb ₂ O ₃	1.1387	Ítrio (Y)	Y ₂ O ₃	1.2699	Lantânio (La)	La ₂ O ₃	1.1728	Lutécio (Lu)	Lu ₂ O ₃	1.1371	Neodímio (Nd)	Nd ₂ O ₃	1.1664	Praseodímio (Pr)	Pr ₆ O ₁₁	1.2082	Samário (Sm)	Sm ₂ O ₃	1.1596	Térbio (Tb)	Tb ₄ O ₇	1.1762	Túlio (Tm)	Tm ₂ O ₃	1.1421
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Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data.	- Data is recorded in the field using a tablet-based GIS system, with some locations also being marked with a Samsung Galaxy Tab Active 5. - Data is uploaded to cloud storage daily and added to CR3's in-house geological database. - Subsequent laboratory assays are verified by the company's Exploration Manager. - Assay data are received in digital format from the laboratory, accompanied by the corresponding locked PDF. - Standard Reference Material sample results are checked from each sample batch to ensure they are within tolerance (<3SD) and that there is no bias. - Assay data yielding elemental concentrations will be converted																																																

Criteria	Explanation	Comment
		to their stoichiometric oxides in a calculation performed within the database using Standard conversion factors. Oxide and elemental values are reported throughout this announcement for completeness.
<i>Location of data points</i>	<i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i> <i>Specification of the grid system used.</i> <i>Quality and adequacy of topographic control.</i>	- Auger hole locations were recorded with a GPS integrated to the Samsung Galaxy Tab Active 5, with a nominal accuracy of +/-3m. - The datum used is UTM SIRGAS2000 Zone 22S. - The accuracy of the locations is sufficient for this stage of exploration.
<i>Data spacing and distribution</i>	<i>Data spacing for reporting of Exploration Results.</i> <i>Whether the data spacing, and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i> <i>Whether sample compositing has been applied.</i>	- Auger holes did not use a systematic grid, being their disposition roughly 200 x 300m, when possible. - No sample compositing has been applied.
<i>Orientation of data in relation to geological structure</i>	<i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i> <i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i>	The relationship between the orientation of mineralized structures and the sample orientation is currently unknown due to limited geological and structural data. As a result, the potential for sampling bias cannot be accurately assessed at this stage of exploration.
<i>Sample security</i>	<i>The measures taken to ensure sample security.</i>	- The samples were collected from the auger drilling and given individual sample numbers for tracking. - The sample chain of custody was overseen by the CR3 geologist in charge of the program. - CR3 company geologist and/ or mining technician were responsible for collecting the samples and transporting them to the company dispatch centre or commercial laboratory.
<i>Audits or reviews</i>	<i>The results of any audits or reviews of sampling techniques and data.</i>	Internal reviews are undertaken.

Section 2: Reporting of Exploration Results

Criteria	Explanation	Comment
<i>Mineral tenement and land tenure status</i>	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	- The Tunas Project is in the Brazilian state of Paraná and consists of two tenements, separated by 2km. The 826036/2024 is 10.32Km² and 826037/2024 is 7.99Km². Both areas are granted by Mineral Agency of Brazil (ANM) for exploration. They are approximately 75km north from the capital city, Curitiba. - The tenements are 100% held by CR3's wholly owned Brazilian subsidiary Mineração Remo Ltda. - Tunas Granted Tenement Listing: 826036/2024, 826037/2024. - The company is not aware of any impediments to obtaining a licence to operate, subject to carrying out appropriate environmental and clearance surveys.
<i>Exploration done by other parties</i>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	There are no records of rare earth exploration activities in the area. The permits belonged to another company, whose main objective was base metal research, but there is no evidence of any field work.
<i>Geology</i>	<i>Deposit type, geological setting and style of mineralisation.</i>	- The Tunas Project is prospective for residual regolith-hosted rare earth mineralisation. The regional geology consists of two distinct units: 1. Tigre granitic to granodioritic orthogneiss, intensely deformed, metamorphosed, and responsible for a strong radiometric anomaly; 2. Metasedimentary succession intercalated by metabasalts, metapsammites, and metapelites of the Votuverava Group. - The granite-gneiss complex is highly weathered, and its residual soil profile was investigated in this sampling phase. - The intrusive rock to the southeast is interpreted to be a Neoproterozoic I-type, calc-alkaline granitoid batholith dominated by monzogranite to granodiorite with biotite ± hornblende. It commonly hosts mafic enclaves and accessory phases such as zircon, apatite and monazite, reflecting magma mixing and fractional crystallisation processes.
<i>Drill hole Information</i>	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: - easting and northing of the drill hole collar - elevation or RL (Reduced Level – elevation above sea level in	Auger holes details are located within Appendix 1 of the ASX release.

Criteria	Explanation	Comment
	metres) of the drill hole collar - dip and azimuth of the hole - down hole length and interception depth - hole length. If the exclusion of this information is justified on the basis that the information is not material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high- g r a d e results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated.	• Weighted averages were used for calculating significant intercepts where the intercepts included samples over intervals of different lengths. • No maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades have been applied.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	• Auger holes are vertical. • True width is not known. All intercepts are reported as down hole length.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include,	• Diagrams are included in the body of this release.

Criteria	Explanation	Comment
	<i>but not be limited to, a plan view of drill hole collar locations and appropriate sectional views.</i>	
<i>Balanced reporting</i>	<i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i>	- All assay results have been reported. - All auger holes are set out in Table in body the report, as well as their intersections (appendix 1, 2 and 3).
<i>Other substantive exploration data</i>	<i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i>	There is no substantive data to report at this stage of exploration.
<i>Further work</i>	<i>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i>	- The next phase of exploration will include diamond drilling to test the full thickness of the weathering profile. - Geophysics (electric tomography) may be utilised to define the weathering profile for drill target vectoring.