ASX Announcement
Media Release

Company Announcements Office
Australian Securities Exchange

EPM 27609 OVER THE WAITARA COPPER AND SILVER PORPHYRY IS GRANTED

FEBRUARY 25, 2021

Duke Exploration (ASX Code: DEX) is pleased to announce that the tenement application (EPM 27609) over the Waitara porphyry 20 km north east of the Bundarra pluton has been granted for five years. This offers additional opportunities based on historic results for resource discoveries through exploration close to the Bundarra project.

Highlights

- *EPM 27609, which covers the Waitara Porphyry prospect, has been granted to Duke Exploration Limited for a term of 5 years from 18 February 2021 to 17 February 2026 over a total area of 6 sub-blocks,*
- *Intersections from the historic drilling drilled between 1972-1979 and not reported to date by the Company include:*
    - 24.0 m from 46.0 m at 0.31 Cu % in W-0,
    - 12.0 m from 74.0 m at 0.43 Cu % in W-01,
    - 44.0 m from 92.0 m at 0.29 Cu % in W-01,
    - 18.0 m from 132.0 m at 0.23 Cu % in W-02,
    - 34.0 m from 44.0 m at 0.26 Cu % in W-08,
    - 16.0 m from 22.0 m at 2.14 Cu % in W-PDH3,
    - 19.0 m from 38.0 m at 0.37 Cu % in W-PDH9,
    - 102.0 m from 28.0 m at 0.22 Cu % in WTDH001,
    - 99.0 m from 11.0 m at 0.35 Cu % in WTDH002.
- *The geology of the tenement is similar to the geology of the Bundarra pluton, but at a smaller scale,*
- *Little exploration has been conducted since the 1970s and most of the historic drillholes are shallow and vertical and are unlikely to have tested the porphyry mineralisation adequately.*
- *No modern geophysics has been carried out on the tenement and therefore there is the potential to identify new drill targets using these techniques. Electrical geophysical methods such as 3D IP*

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and VTEM have been shown to accurately map sulphide mineralisation at Bundarra and similar methods could be successful at Waitara.

- *Based on laboratory turnaround times to date, the results from the next line to the south are expected to be finalised for announcing by early-March, the results of the line to the north by mid-March and the results from the drilling of the three holes into the VTEM anomaly by early April,*
- *Electrical geophysical surveys and pXRF soil sampling to follow up and test the extensions of the anomalies discovered at Quorn continued, with results expected by the end of March.*

Details of the work reported in this announcement are outlined in Appendix 1 - JORC Code , 2012 Edition, Checklist of Assessment and Reporting Criteria.

Commenting on progress - Toko Kapea, Chairman:

"We are pleased to have the Waitara tenement granted as this will allow us to get on the ground to confirm the interesting historic exploration results from past explorers. Waitara is only 20 km to the east of Bundarra with the main access on sealed roads, so any discovery could easily be transported to Bundarra that would add to the potential resource base that is being developed from our exciting results to date. We look forward to adding resources from this new opportunity in the future and like Bundarra expect a few surprises along the way. "

Q1 and Q2 Work Programmes

- *Continue the phase two infill drilling at Mt Flora guided by the results from the phase one drilling,*
- *Complete pattern resource drilling at the Quarry Anomaly focussing on the higher grade northern strike extension (this drilling has started),*
- *Complete follow up geophysics surveys at Quorn to allow planning of a drilling programme to test the results from this work,*
- *Extend the gradient array and pXRF soil sampling to cover anomalous areas from the Quorn surveys that are open,*
- *Complete gradient array and pXRF soil surveys over the Isens Underground mine area, with the aim of starting drill testing by the second quarter of 2021,*
- *Finalise land access and drill planning at the Prairie Creek gold target,*
- *Source a second rig to fast-track resource and exploration drilling over Mt Flora, Quorn and the Quarry prospects.*

This announcement has been authorised for release by the Board.

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Technical Information

Waitara Porphyry Prospect

The Waitara Porphyry prospect is covered by EPM 27609, which has been granted to Duke Exploration Limited for a term of 5 years from 18 February 2021 to 17 February 2026 over a total area of 6 sub-blocks. The tenement now forms part of the Bundarra project in eastern Central Queensland, 80 km southwest of Mackay and the tenement is 20 km northeast of Bundarra (Figure 1). Access to the area is via the Bruce Highway from Mackay to Sarina (35 km), and then via minor roads to the project area (80 km).

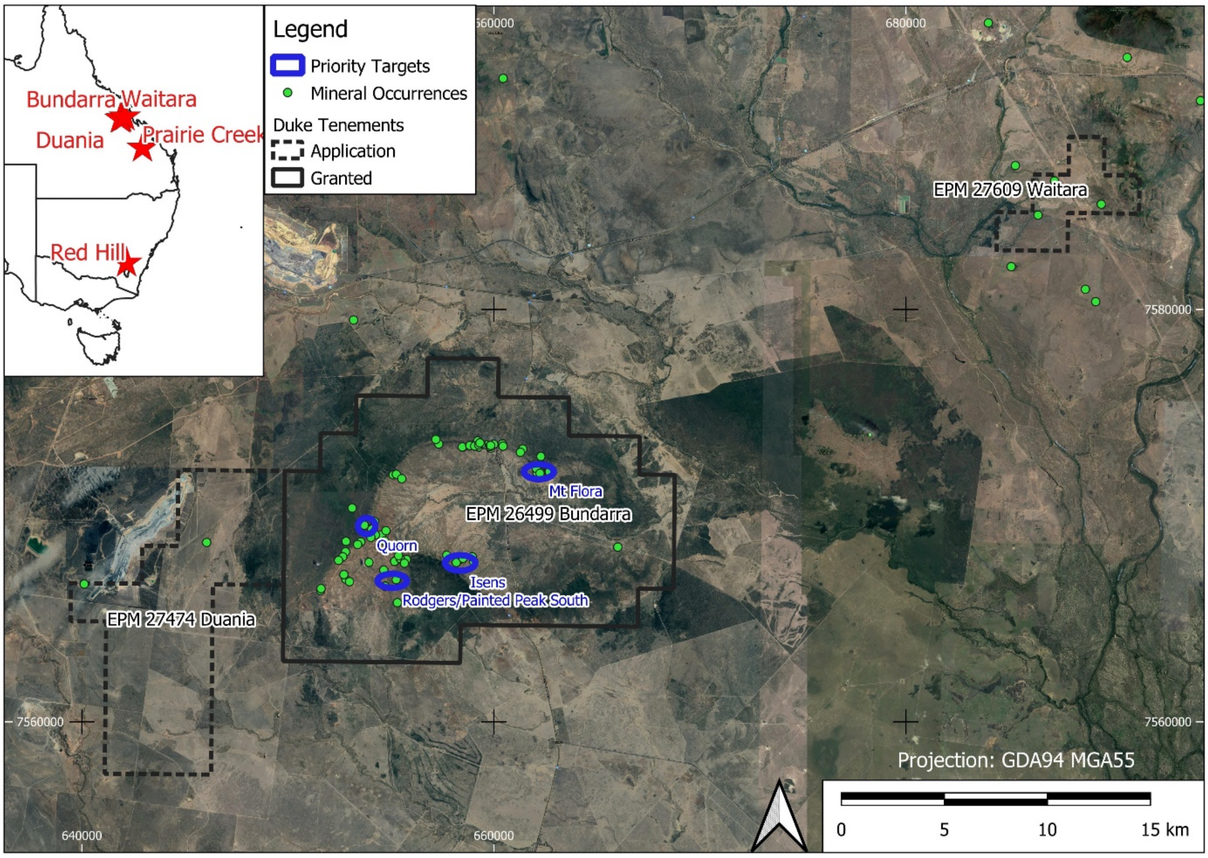

Figure 1: Location of Bundarra Project (EPM 26499 (Bundarra), EPM 27474 (Duania) and EMP 27609 (Waitara)) compared to historic prospects and main target areas.

EPM 27609 is located on the eastern margin of the Bowen Basin and covers similar age geology to the Bundarra tenement 20 km to the west. The east of the tenement, including the Waitara Porphyry prospect, comprises Devonian-Carboniferous felsic to intermediate volcanics (lava, ignimbrite, tuff, agglomerate, and volcanic sediments) and subordinate granite. There is poor outcrop to the west of the tenement, which is flat-lying and covered by Cainozoic alluvium and Tertiary basalt. The Devonian-Carboniferous lithologies are unconformably overlain by Lizzie Creek Volcanics that comprise west-dipping andesite and sediments, which are themselves unconformably overlain by marine Bowen Basin sediments. The Lizzie Creek Volcanics are Early Permian in age and are unconformably overlain by a Lower Permian sequence of fine-grained sediments and mafic volcanics that represent the first true succession of the Bowen Basin coal measures.

The Waitara Granite crops out 200 m north of the Waitara Porphyry prospect, and is a pinkish-grey, fine to medium-grained, porphyritic biotite-hornblende monzonite to monzogranite with plagioclase and hornblende phenocrysts and is assigned an early Cretaceous age similar to Bundarra (Figure 2). The granodiorite contains numerous roof pendants, indicating that the rocks exposed at the surface represent the top of an intrusive body. The host Permian lithologies are crosscut by post-mineral porphyritic diorite and granodiorite dykes and overlain by andesitic tuff and ignimbrite (Figure 2). The porphyry is locally covered by a silicified volcanic cap that contains abundant fracture filling and disseminated limonite, reflecting weathering of sulfides that comprised 1-5 vol% of the un-weathered rocks. Traces of copper oxide mineralisation occurs within the cap rocks and they are also variably affected by sericite and clay alteration.

There are three historic prospects located within the tenement that have been the focus for historic exploration (Figure and Figure 2). The Waitara Porphyry Prospect is the most advanced with the most work done to date. The major metallic minerals described from the exploration to date are pyrite, chalcopyrite, molybdenite and magnetite. Phyllic and propylitic alteration are common but potassic alteration is rare and supergene enrichment is weak.

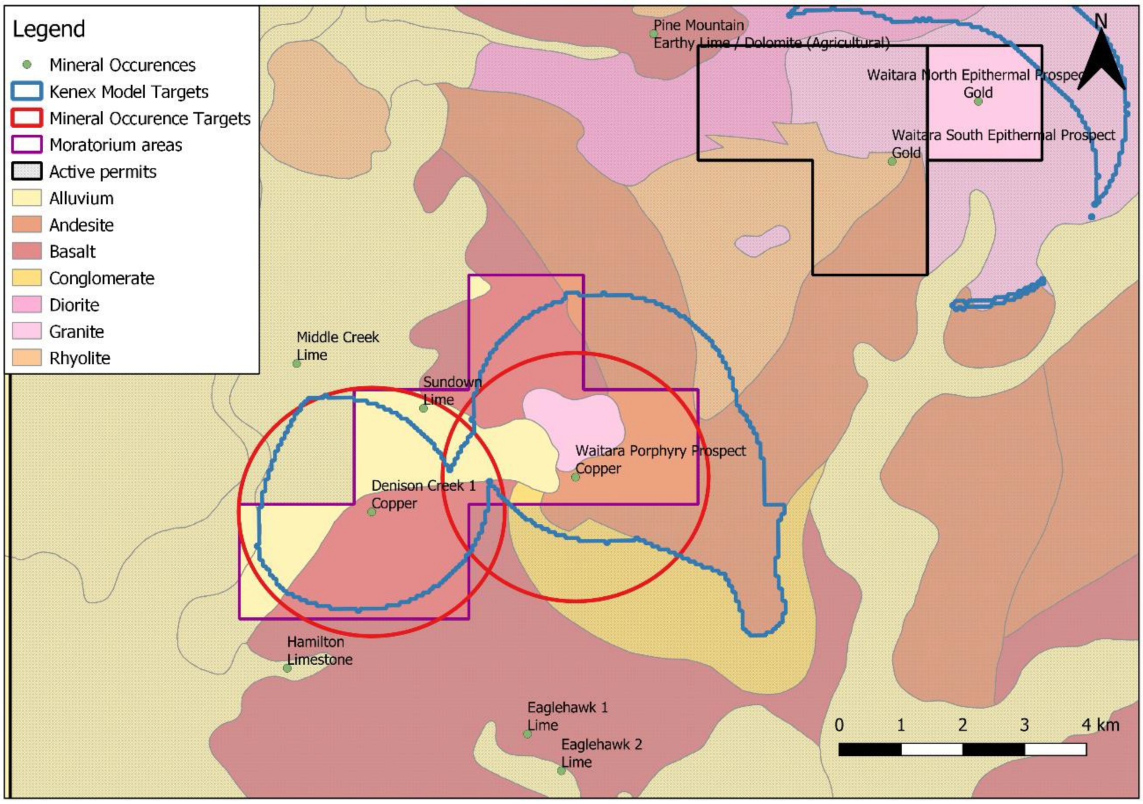

Figure 2. Geology map of the Waitara prospect tenement EMP 27609.

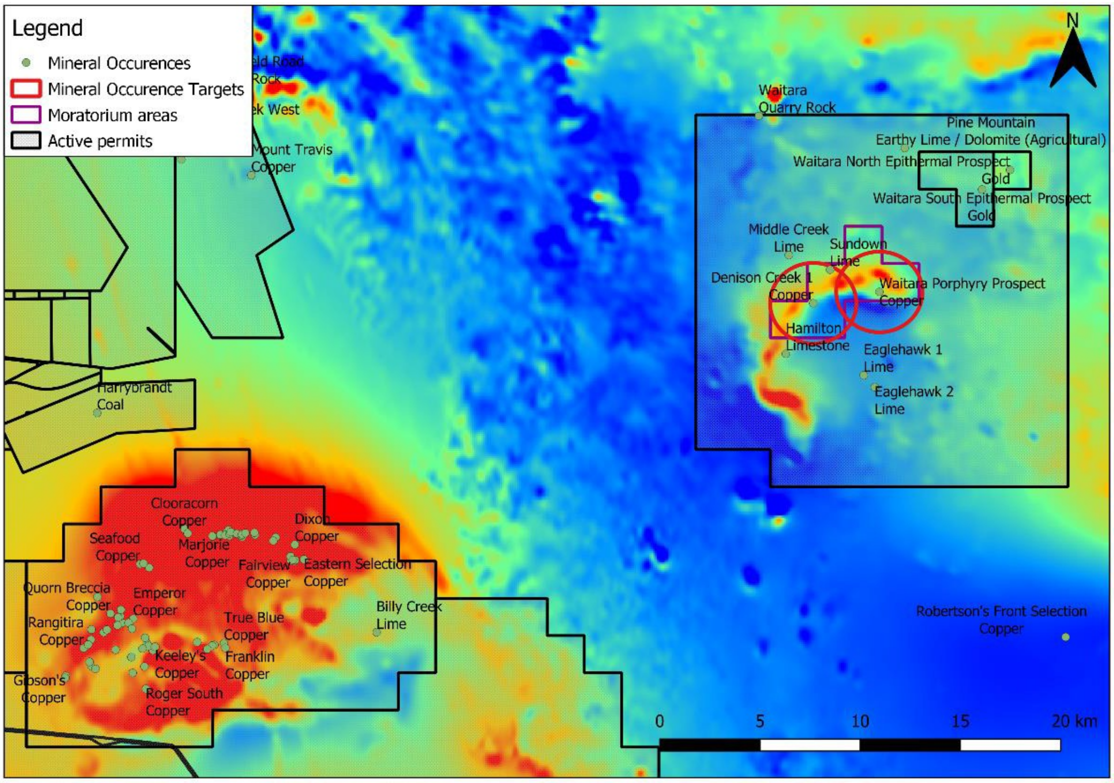

Figure 3. State-wide magnetic imagery (TMI) over the Bundarra and Waitara tenements.

The prospects in EMP 27609 occur along the edge of a well-defined arcuate magnetic high that encloses a circular magnetic low (Figure 3), which is interpreted to be a buried intrusion like Bundarra. The signature of the magnetic high is similar to that of the Bundarra granodiorite and may represent a later, more mafic magma that intruded along the margin of an older more felsic intrusive body.

All available historic exploration data have been compiled for the Waitara tenement area and integrated into the Bundarra project databases. The data collected include 631 drillholes, 575 soil samples, 179 stream sediment samples, 85 rock chips, several geology maps and cross-sections, gridded magnetic-radiometric data, and several historic geophysical images. The data have been checked and QAQC carried out, with the data being reasonable quality.

A total of 631 drillholes have been completed in the tenement area for a total of 6,724m of drilling (Figure and Appendix 1). Most are shallow RAB holes, with only 18 holes drilled past 60m down hole (Appendix 1). Better intersections from the deeper holes that are listed in full in Appendix 2 include:

- 24.0 m from 46.0 m at 0.31 Cu % in W-0,
- 12.0 m from 74.0 m at 0.43 Cu % in W-01,
- 44.0 m from 92.0 m at 0.29 Cu % in W-01,
- 18.0 m from 132.0 m at 0.23 Cu % in W-02,
- 34.0 m from 44.0 m at 0.26 Cu % in W-08,
- 16.0 m from 22.0 m at 2.14 Cu % in W-PDH3,
- 19.0 m from 38.0 m at 0.37 Cu % in W-PDH9,
- 102.0 m from 28.0 m at 0.22 Cu % in WTDH001,
- 99.0 m from 11.0 m at 0.35 Cu % in WTDH002.

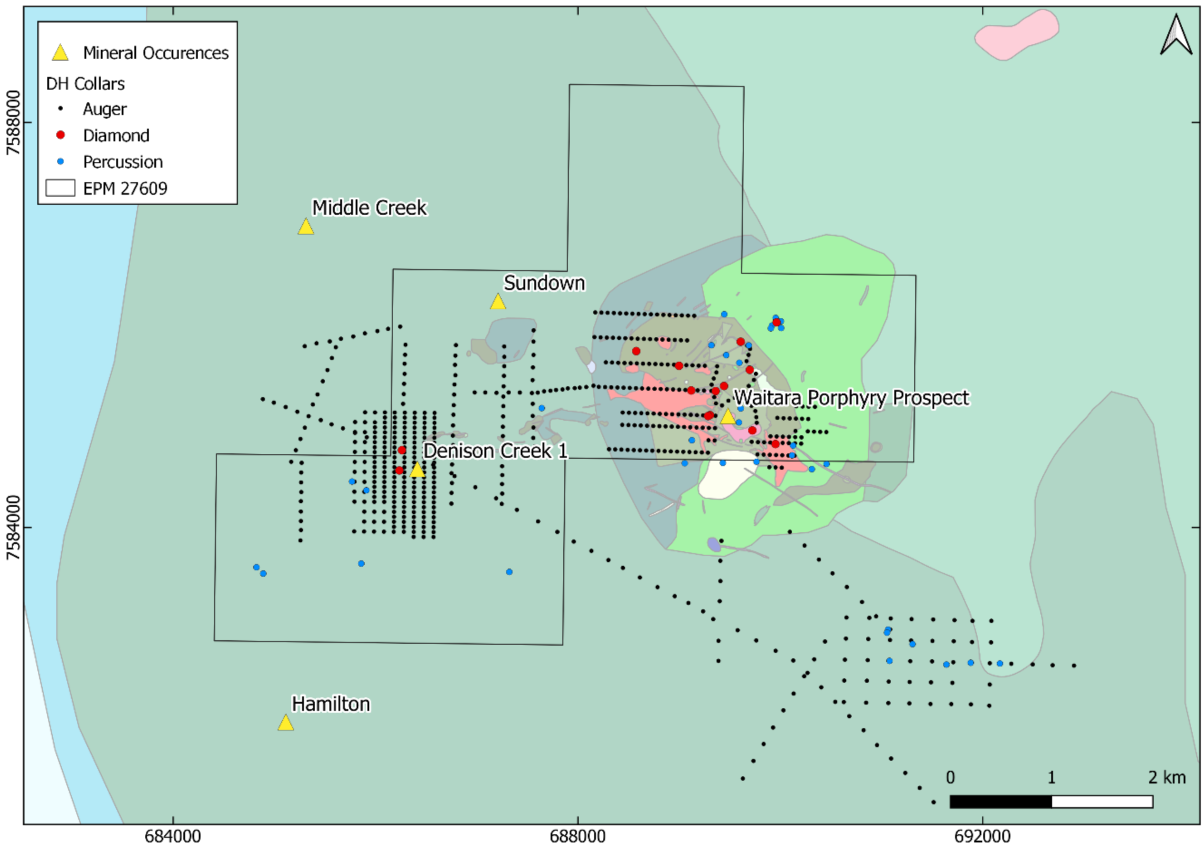

Figure 4. Historic collar locations and hole types of holes drilled between 1972 and 1979 compiled over the granted Waitara tenement area listed in Appendix 1.

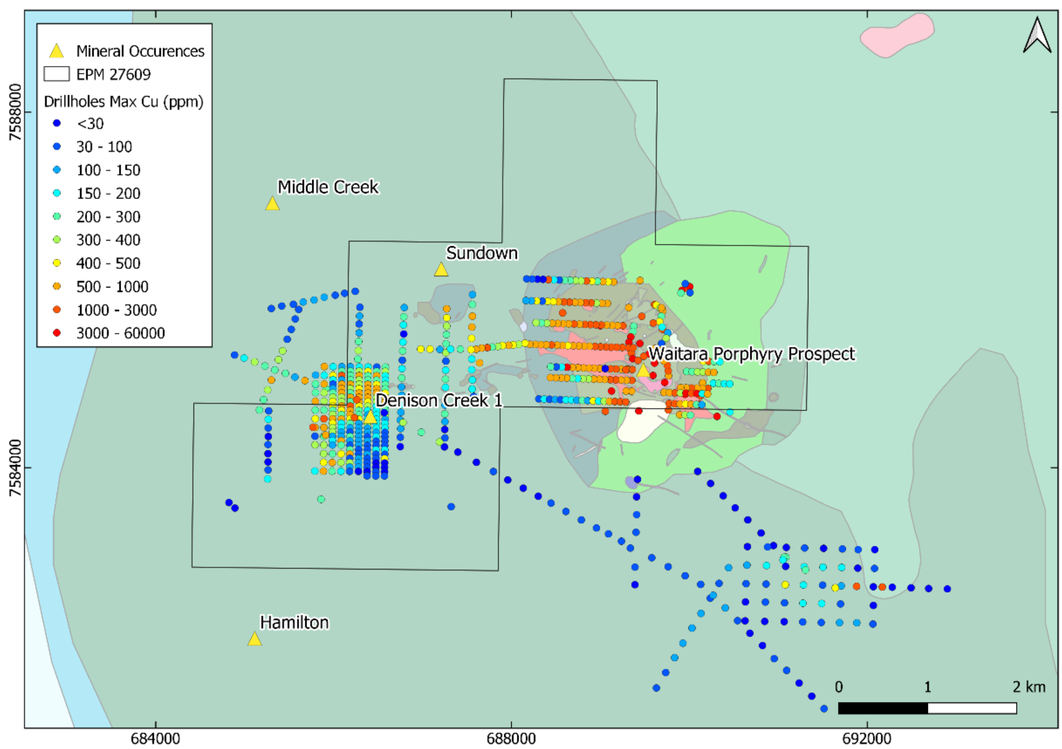

Figure 5. Historic drillholes drilled between 1972-1979 coloured by maximum copper assay listed in Appendix 1.

All but two of the historic drill holes were drilled between 1972 and 1979 under EPM 1091. Most holes intersected significant copper mineralisation associated with elevated molybdenum (Figure 5 and Appendix 1). Importantly most holes were only assayed for copper and molybdenum and therefore the total metal endowment of the deposit is not well understood. Only 82 samples from 12 percussion holes were assayed for gold; one sample returned 0.1 ppm Au and the rest were below the detection limit (0.1 ppm Au). A total of 582 samples were analysed for silver (only 20% of the total number of samples), with a maximum assay of 640 ppm Ag, which is similar to the mineralisation at Bundarra. The highest copper grades were returned from W-PDH3, a percussion hole drilled at the Waitara Porphyry prospect, that intersected 16 m @ 2.14% Cu, including 2 m at 6.0 % Cu from 22 m down hole. The deeper holes into the Waitara Porphyry intersected wide intervals of low-grade copper mineralisation. For example, the whole length of W-01 was mineralised, returning 305 m @ 0.2% Cu and 69 ppm Mo (Appendix 2). Some of the holes at Denison Creek intersected significant copper mineralisation as listed in Appendix 2. However, the results were generally less encouraging than Waitara. The copper intersected to date defines a 2 km^2 zone of copper mineralisation around the Waitara Porphyry Prospect and a smaller area around Denison Creek (Figure).

The historic data confirm the initial assessment that the Waitara tenement is highly prospective for porphyry copper-molybdenum mineralisation similar to that currently being explored at Bundarra. The Waitara Porphyry Prospect is clearly the main target in the tenement, having returned several encouraging drill intersections of broad, low-grade Cu-Mo mineralisation and adds another target for development to the Bundarra project.

Little exploration has been conducted in the area since the 1970s, most of the drillholes are shallow and vertical and are therefore unlikely to have completely tested the potential of the tenement. No modern geophysics has been carried out at Waitara and therefore there is the potential to identify new drill targets using these techniques. Electrical geophysical methods such as 3D IP and VTEM have been shown to accurately map sulphide mineralisation at Bundarra and similar methods would likely be successful at Waitara.

About Duke Exploration

Duke is an Australian exploration company with majority interests in five granted exploration tenements for copper, gold and silver exploration areas located in Queensland and New South Wales, Australia.

Duke’s key assets comprise:

- EPM26499, EPM2747 and EPM 27609 – Bundarra Project (100% owned copper exploration project near Mackay, Queensland),
- EPM 26852 – Prairie Creek Project (91% owned (9% Capgold) gold exploration project near Rockhampton, Queensland), and
- EL 8568 – Red Hill Project (100% owned copper exploration project near Red Hill, New South Wales).

In addition, Duke also has an interest in four New South Wales Cu-Au porphyry tenements currently operated by Lachlan Resources Pty Ltd, a wholly owned subsidiary of ASX listed Emmerson Resources (ASX:ERM). Duke currently holds a 5% interest in two of these tenements and a 10% interest in the other two tenements that is free carried to BFS.

The highest priority target for the Company is the Mt Flora Prospect in the Bundarra Project, one of the numerous Bundarra Project's prospects, which has resource development potential for copper, silver and gold. All historic data from the mine at the Mt Flora Prospect has been checked in the field by diamond drilling and ground geophysics, which have confirmed the tenor and scale of copper, silver and gold mineralisation mined previously. There are five other areas with similar development potential on the Bundarra Project as defined by historic mining, geology and geophysics.

Our aim in the next two years is to develop an Indicated Mineral Resource at the Mt Flora Prospect to allow feasibility studies to be undertaken and o delineate additional Inferred Mineral Resources from the current known exploration target areas. The Company also intends to drill the more conceptual exploration targets on the Prairie Creek Project and Red Hill Project (see www.duke-exploration.com.au for more project details).

Competent person statement

The information in the ASX announcement is based on information compiled by Dr Gregor Partington, who is a Member of The Australasian Institute of Mining and Metallurgy and a Member of the Australian Institute of Geoscientists. Dr Gregor Partington has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' (the JORC Code).

Dr Gregor Partington is engaged by Duke Exploration as Operations Manager and consents to the inclusion of the information in the ASX announcement in the form and context in which it appears.

Appendix 1 – Waitara historic drill hole details (MGA94 Zone 55)

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
CL-0000	RAB	690,442	7,582,873	3.7	360	-90	110
CL-0200	RAB	690,335	7,582,697	3.7	360	-90	46
CL-0400	RAB	690,236	7,582,530	3.7	360	-90	100
CL-0600	RAB	690,132	7,582,359	3.7	360	-90	120
CL-0800	RAB	690,031	7,582,194	3.7	360	-90	125
CL-1000	RAB	689,929	7,582,024	3.7	360	-90	135
CL-1200	RAB	689,835	7,581,861	3.7	360	-90	125
CL-1400	RAB	689,735	7,581,694	3.7	360	-90	100
CL-1600	RAB	689,630	7,581,520	3.7	360	-90	45
DC01	RAB	685,913	7,584,891	2.4	360	-90	270
DC02	RAB	685,797	7,584,934	3.7	360	-90	170
DC03	RAB	685,677	7,584,979	3.7	360	-90	535
DC04	RAB	685,565	7,585,018	3.7	360	-90	110
DC05	RAB	685,459	7,585,060	3.7	360	-90	270
DC06	RAB	685,338	7,585,098	3.7	360	-90	265
DC07	RAB	685,227	7,585,142	3.7	360	-90	285
DC08	RAB	685,111	7,585,189	3.7	360	-90	310
DC09	RAB	684,994	7,585,233	2.4	360	-90	180
DC10	RAB	684,886	7,585,267	4.3	360	-90	50
DC11	RAB	685,301	7,584,985	3.7	360	-90	760
DC12	RAB	685,258	7,584,874	3.7	360	-90	320
DC13	RAB	685,212	7,584,763	3.7	360	-90	285
DC14	RAB	685,166	7,584,648	3.7	360	-90	205
DC15	RAB	685,380	7,585,214	3.7	360	-90	380
DC16	RAB	685,426	7,585,313	3.7	360	-90	385
DC17	RAB	685,478	7,585,444	3.7	360	-90	100
DC18	RAB	685,525	7,585,555	3.7	360	-90	85
DC19	RAB	685,568	7,585,673	3.7	360	-90	85
DC20	RAB	685,607	7,585,780	3.7	360	-90	45
DC21	RAB	685,658	7,585,863	3.7	360	-90	150
DC22	RAB	685,548	7,585,837	3.7	360	-90	35
DC23	RAB	685,417	7,585,818	3.7	360	-90	60
DC24	RAB	685,300	7,585,790	3.7	360	-90	55
DC26	RAB	685,779	7,585,886	3.7	360	-90	135
DC27	RAB	685,894	7,585,917	3.7	360	-90	135
DC28	RAB	686,018	7,585,940	3.7	360	-90	60
DC29	RAB	686,124	7,585,961	3.7	360	-90	70
DC30	RAB	686,243	7,585,983	3.7	360	-90	55
DC1000	RAB	685,270	7,584,638	3.7	360	-90	80
DC1001	RAB	685,265	7,584,543	3.7	360	-90	200
DC1002	RAB	685,264	7,584,445	3.7	360	-90	40
DC1003	RAB	685,266	7,584,350	3.7	360	-90	25
DC1004	RAB	685,262	7,584,259	3.7	360	-90	35
DC1005	RAB	685,262	7,584,157	3.7	360	-90	20

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
DC1006	RAB	685,262	7,584,063	3.7	360	-90	25
DC1007	RAB	685,263	7,583,974	3.7	360	-90	35
DC1008	RAB	685,258	7,583,871	3.7	360	-90	200
DC1009	RAB	686,296	7,585,804	3.7	360	-90	95
DC1010	RAB	686,292	7,585,705	3.7	360	-90	120
DC1011	RAB	686,287	7,585,617	3.7	360	-90	85
DC1012	RAB	686,287	7,585,517	3.7	360	-90	135
DC1013	RAB	686,281	7,585,418	3.7	360	-90	250
DC1014	RAB	686,278	7,585,317	3.7	360	-90	380
DC1015	RAB	686,272	7,585,221	3.7	360	-90	250
DC1016	RAB	686,794	7,585,800	3.7	360	-90	105
DC1017	RAB	686,789	7,585,697	3.7	360	-90	250
DC1018	RAB	686,785	7,585,606	3.7	360	-90	180
DC1019	RAB	686,789	7,585,503	3.7	360	-90	0
DC1020	RAB	686,780	7,585,412	3.7	360	-90	200
DC1021	RAB	686,777	7,585,312	3.7	360	-90	300
DC1022	RAB	686,772	7,585,208	3.7	360	-90	75
DC1023	RAB	686,769	7,585,113	3.7	360	-90	180
DC1024	RAB	686,766	7,585,008	3.7	360	-90	300
DC1025	RAB	686,764	7,584,907	3.7	360	-90	140
DC1026	RAB	686,766	7,584,813	3.7	360	-90	135
DC1027	RAB	686,756	7,584,707	3.7	360	-90	200
DC1028	RAB	686,756	7,584,622	3.7	360	-90	130
DC1029	RAB	686,750	7,584,535	3.7	360	-90	150
DC1030	RAB	686,755	7,584,438	3.7	360	-90	120
DC1031	RAB	686,751	7,584,341	3.7	360	-90	70
DC1032	RAB	686,750	7,584,235	3.7	360	-90	25
DC1033	RAB	687,271	7,585,787	3.7	360	-90	660
DC1034	RAB	687,272	7,585,685	3.7	360	-90	450
DC1035	RAB	687,272	7,585,592	3.7	360	-90	380
DC1036	RAB	687,269	7,585,497	3.7	360	-90	300
DC1037	RAB	687,266	7,585,394	3.7	360	-90	280
DC1038	RAB	687,263	7,585,293	3.7	360	-90	400
DC1039	RAB	687,263	7,585,198	3.7	360	-90	60
DC1040	RAB	687,261	7,585,096	3.7	360	-90	160
DC1041	RAB	687,258	7,584,994	3.7	360	-90	240
DC1042	RAB	687,258	7,584,902	3.7	360	-90	195
DC1045	RAB	687,253	7,584,703	3.7	360	-90	120
DC1046	RAB	687,251	7,584,605	3.7	360	-90	220
DC1047	RAB	687,252	7,584,517	3.7	360	-90	105
DC1048	RAB	687,250	7,584,428	3.7	360	-90	25
DC1049	RAB	687,252	7,584,334	3.7	360	-90	35
DC1050	RAB	687,247	7,584,232	3.7	360	-90	20
DC1063	RAB	687,576	7,584,801	3.7	360	-90	100
DC-101	RAB	685,797	7,585,041	3.7	360	-90	130
DC-102	RAB	685,796	7,584,942	3.7	360	-90	270

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
DC-103	RAB	685,796	7,584,844	3.7	360	-90	270
DC-104	RAB	685,795	7,584,746	3.7	360	-90	920
DC-105	RAB	685,794	7,584,647	3.7	360	-90	210
DC-106	RAB	685,793	7,584,549	3.7	360	-90	430
DC-107	RAB	685,792	7,584,452	3.7	360	-90	1,000
DC-108	RAB	685,790	7,584,353	3.7	360	-90	100
DC-109	RAB	685,791	7,584,255	3.7	360	-90	370
DC-110	RAB	685,788	7,583,961	3.7	360	-90	200
DC-111	RAB	685,896	7,585,137	3.7	360	-90	700
DC-112	RAB	685,895	7,585,039	3.7	360	-90	200
DC-113	RAB	685,894	7,584,941	3.7	360	-90	600
DC-114	RAB	685,894	7,584,843	3.7	360	-90	320
DC-115	RAB	685,893	7,584,745	3.7	360	-90	360
DC-116	RAB	685,892	7,584,647	3.7	360	-90	290
DC-117	RAB	685,891	7,584,549	3.7	360	-90	1,100
DC-118	RAB	685,890	7,584,450	3.7	360	-90	880
DC-119	RAB	685,889	7,584,352	3.7	360	-90	270
DC-120	RAB	685,889	7,584,254	3.7	360	-90	310
DC-121	RAB	685,888	7,584,156	3.7	360	-90	320
DC-122	RAB	685,887	7,584,058	3.7	360	-90	440
DC-123	RAB	685,886	7,583,960	3.7	360	-90	580
DC-124	RAB	685,994	7,585,136	3.7	360	-90	175
DC-125	RAB	685,993	7,585,038	3.7	360	-90	430
DC-126	RAB	685,993	7,584,989	3.7	360	-90	200
DC-127	RAB	685,993	7,584,940	3.7	360	-90	80
DC-128	RAB	685,992	7,584,891	3.7	360	-90	150
DC-129	RAB	685,992	7,584,842	3.7	360	-90	230
DC-130	RAB	685,991	7,584,792	3.7	360	-90	350
DC-131	RAB	685,991	7,584,744	3.7	360	-90	500
DC-132	RAB	685,990	7,584,695	3.7	360	-90	430
DC-133	RAB	685,990	7,584,645	3.7	360	-90	260
DC-134	RAB	685,990	7,584,597	3.7	360	-90	360
DC-135	RAB	685,989	7,584,548	3.7	360	-90	570
DC-136	RAB	685,989	7,584,499	3.7	360	-90	430
DC-137	RAB	685,988	7,584,450	3.7	360	-90	350
DC-138	RAB	685,988	7,584,401	3.7	360	-90	350
DC-139	RAB	685,988	7,584,352	3.7	360	-90	120
DC-140	RAB	685,987	7,584,302	3.7	360	-90	175
DC-141	RAB	685,987	7,584,253	3.7	360	-90	130
DC-142	RAB	685,987	7,584,155	3.7	360	-90	280
DC-143	RAB	685,985	7,584,056	3.7	360	-90	1,000
DC-144	RAB	685,984	7,583,959	3.7	360	-90	210
DC-145	RAB	686,092	7,585,136	3.7	360	-90	110
DC-146	RAB	686,092	7,585,086	3.7	360	-90	220
DC-147	RAB	686,091	7,585,037	3.7	360	-90	1,700
DC-148	RAB	686,091	7,584,988	3.7	360	-90	110

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
DC-149	RAB	686,092	7,584,939	3.7	360	-90	540
DC-150	RAB	686,090	7,584,890	3.7	360	-90	520
DC-151	RAB	686,090	7,584,841	3.7	360	-90	660
DC-152	RAB	686,089	7,584,792	3.7	360	-90	360
DC-153	RAB	686,089	7,584,743	3.7	360	-90	310
DC-154	RAB	686,089	7,584,694	3.7	360	-90	600
DC-155	RAB	686,088	7,584,645	3.7	360	-90	450
DC-156	RAB	686,088	7,584,596	3.7	360	-90	300
DC-157	RAB	686,087	7,584,547	3.7	360	-90	820
DC-158	RAB	686,087	7,584,498	3.7	360	-90	165
DC-159	RAB	686,086	7,584,449	3.7	360	-90	170
DC-160	RAB	686,086	7,584,400	3.7	360	-90	150
DC-161	RAB	686,086	7,584,351	3.7	360	-90	135
DC-162	RAB	686,085	7,584,302	3.7	360	-90	1,000
DC-163	RAB	686,085	7,584,253	3.7	360	-90	220
DC-164	RAB	686,084	7,584,154	3.7	360	-90	420
DC-165	RAB	686,083	7,584,056	3.7	360	-90	340
DC-166	RAB	686,082	7,583,958	3.7	360	-90	200
DC-167	RAB	686,189	7,585,135	3.7	360	-90	120
DC-168	RAB	686,190	7,585,086	3.7	360	-90	240
DC-169	RAB	686,190	7,585,037	3.7	360	-90	260
DC-170	RAB	686,189	7,584,988	3.7	360	-90	290
DC-171	RAB	686,189	7,584,938	3.7	360	-90	640
DC-172	RAB	686,188	7,584,889	3.7	360	-90	340
DC-173	RAB	686,188	7,584,840	3.7	360	-90	260
DC-174	RAB	686,187	7,584,791	3.7	360	-90	1,000
DC-175	RAB	686,187	7,584,742	3.7	360	-90	240
DC-176	RAB	686,187	7,584,693	3.7	360	-90	1,600
DC-177	RAB	686,186	7,584,644	3.7	360	-90	640
DC-178	RAB	686,186	7,584,595	3.7	360	-90	660
DC-179	RAB	686,185	7,584,547	3.7	360	-90	490
DC-180	RAB	686,185	7,584,497	3.7	360	-90	240
DC-181	RAB	686,185	7,584,448	3.7	360	-90	150
DC-182	RAB	686,184	7,584,400	3.7	360	-90	55
DC-183	RAB	686,184	7,584,350	3.7	360	-90	220
DC-184	RAB	686,183	7,584,301	3.7	360	-90	120
DC-185	RAB	686,183	7,584,252	3.7	360	-90	100
DC-186	RAB	686,183	7,584,203	3.7	360	-90	240
DC-187	RAB	686,182	7,584,154	3.7	360	-90	860
DC-188	RAB	686,182	7,584,105	3.7	360	-90	70
DC-189	RAB	686,181	7,584,056	3.7	360	-90	380
DC-190	RAB	686,181	7,584,006	3.7	360	-90	115
DC-191	RAB	686,179	7,583,957	3.7	360	-90	50
DC-192	RAB	686,289	7,585,134	3.7	360	-90	200
DC-193	RAB	686,288	7,585,085	3.7	360	-90	320
DC-194	RAB	686,288	7,585,036	3.7	360	-90	600

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
DC-195	RAB	686,287	7,584,987	3.7	360	-90	370
DC-196	RAB	686,287	7,584,938	3.7	360	-90	390
DC-197	RAB	686,286	7,584,889	3.7	360	-90	500
DC-198	RAB	686,286	7,584,840	3.7	360	-90	740
DC-199	RAB	686,286	7,584,790	3.7	360	-90	720
DC-200	RAB	686,284	7,584,741	3.7	360	-90	740
DC-201	RAB	686,285	7,584,692	3.7	360	-90	430
DC-202	RAB	686,284	7,584,643	3.7	360	-90	250
DC-203	RAB	686,284	7,584,594	3.7	360	-90	220
DC-204	RAB	686,284	7,584,545	3.7	360	-90	500
DC-205	RAB	686,283	7,584,496	3.7	360	-90	125
DC-206	RAB	686,283	7,584,447	3.7	360	-90	105
DC-207	RAB	686,282	7,584,398	3.7	360	-90	120
DC-208	RAB	686,282	7,584,349	3.7	360	-90	110
DC-209	RAB	686,281	7,584,300	3.7	360	-90	105
DC-210	RAB	686,281	7,584,251	3.7	360	-90	115
DC-211	RAB	686,281	7,584,202	3.7	360	-90	100
DC-212	RAB	686,280	7,584,153	3.7	360	-90	70
DC-213	RAB	686,280	7,584,104	3.7	360	-90	105
DC-214	RAB	686,279	7,584,055	3.7	360	-90	120
DC-215	RAB	686,279	7,584,006	3.7	360	-90	120
DC-216	RAB	686,279	7,583,957	3.7	360	-90	30
DC-217	RAB	686,387	7,585,133	3.7	360	-90	200
DC-218	RAB	686,386	7,585,084	3.7	360	-90	490
DC-219	RAB	686,386	7,585,035	3.7	360	-90	210
DC-220	RAB	686,385	7,584,986	3.7	360	-90	240
DC-221	RAB	686,385	7,584,937	3.7	360	-90	720
DC-222	RAB	686,385	7,584,888	3.7	360	-90	560
DC-223	RAB	686,384	7,584,839	3.7	360	-90	660
DC-224	RAB	686,384	7,584,790	3.7	360	-90	1,000
DC-225	RAB	686,383	7,584,740	3.7	360	-90	470
DC-226	RAB	686,383	7,584,692	3.7	360	-90	340
DC-227	RAB	686,382	7,584,642	3.7	360	-90	200
DC-228	RAB	686,382	7,584,592	3.7	360	-90	140
DC-229	RAB	686,382	7,584,544	3.7	360	-90	155
DC-230	RAB	686,381	7,584,495	3.7	360	-90	320
DC-231	RAB	686,381	7,584,446	3.7	360	-90	130
DC-232	RAB	686,380	7,584,397	3.7	360	-90	105
DC-233	RAB	686,379	7,584,348	3.7	360	-90	95
DC-234	RAB	686,380	7,584,299	3.7	360	-90	130
DC-235	RAB	686,379	7,584,250	3.7	360	-90	40
DC-236	RAB	686,379	7,584,201	3.7	360	-90	35
DC-237	RAB	686,378	7,584,151	3.7	360	-90	120
DC-238	RAB	686,378	7,584,103	3.7	360	-90	70
DC-239	RAB	686,377	7,584,054	3.7	360	-90	45
DC-240	RAB	686,377	7,584,004	3.7	360	-90	40

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
DC-241	RAB	686,377	7,583,956	3.7	360	-90	30
DC-242	RAB	686,376	7,583,907	3.7	360	-90	45
DC-243	RAB	686,485	7,585,132	3.7	360	-90	100
DC-244	RAB	686,484	7,585,083	3.7	360	-90	210
DC-245	RAB	686,484	7,585,034	3.7	360	-90	600
DC-246	RAB	686,483	7,584,985	3.7	360	-90	270
DC-247	RAB	686,483	7,584,936	3.7	360	-90	500
DC-248	RAB	686,483	7,584,887	3.7	360	-90	760
DC-249	RAB	686,482	7,584,838	3.7	360	-90	540
DC-250	RAB	686,482	7,584,789	3.7	360	-90	335
DC-251	RAB	686,481	7,584,740	3.7	360	-90	350
DC-252	RAB	686,481	7,584,691	3.7	360	-90	165
DC-253	RAB	686,481	7,584,642	3.7	360	-90	185
DC-254	RAB	686,480	7,584,593	3.7	360	-90	170
DC-255	RAB	686,480	7,584,544	3.7	360	-90	180
DC-256	RAB	686,479	7,584,495	3.7	360	-90	175
DC-257	RAB	686,479	7,584,445	3.7	360	-90	175
DC-258	RAB	686,478	7,584,396	3.7	360	-90	120
DC-259	RAB	686,478	7,584,347	3.7	360	-90	170
DC-260	RAB	686,478	7,584,298	3.7	360	-90	100
DC-261	RAB	686,477	7,584,249	3.7	360	-90	70
DC-262	RAB	686,477	7,584,200	3.7	360	-90	170
DC-263	RAB	686,476	7,584,151	3.7	360	-90	55
DC-264	RAB	686,476	7,584,102	3.7	360	-90	40
DC-265	RAB	686,476	7,584,053	3.7	360	-90	30
DC-266	RAB	686,475	7,584,004	3.7	360	-90	15
DC-267	RAB	686,475	7,583,955	3.7	360	-90	50
DC-268	RAB	686,474	7,583,906	3.7	360	-90	60
DC-269	RAB	686,583	7,585,131	3.7	360	-90	260
DC-270	RAB	686,582	7,585,083	3.7	360	-90	380
DC-271	RAB	686,582	7,585,033	3.7	360	-90	165
DC-272	RAB	686,582	7,584,984	3.7	360	-90	165
DC-273	RAB	686,581	7,584,936	3.7	360	-90	280
DC-274	RAB	686,581	7,584,886	3.7	360	-90	260
DC-275	RAB	686,580	7,584,837	3.7	360	-90	410
DC-276	RAB	686,580	7,584,788	3.7	360	-90	560
DC-277	RAB	686,579	7,584,739	3.7	360	-90	780
DC-278	RAB	686,579	7,584,690	3.7	360	-90	210
DC-279	RAB	686,579	7,584,641	3.7	360	-90	270
DC-280	RAB	686,578	7,584,592	3.7	360	-90	400
DC-281	RAB	686,578	7,584,543	3.7	360	-90	120
DC-282	RAB	686,577	7,584,495	3.7	360	-90	200
DC-283	RAB	686,577	7,584,445	3.7	360	-90	155
DC-284	RAB	686,577	7,584,396	3.7	360	-90	65
DC-285	RAB	686,576	7,584,347	3.7	360	-90	75
DC-286	RAB	686,576	7,584,297	3.7	360	-90	70

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
DC-287	RAB	686,575	7,584,248	3.7	360	-90	40
DC-288	RAB	686,575	7,584,199	3.7	360	-90	200
DC-289	RAB	686,575	7,584,150	3.7	360	-90	40
DC-290	RAB	686,574	7,584,101	3.7	360	-90	440
DC-291	RAB	686,574	7,584,052	3.7	360	-90	30
DC-292	RAB	686,573	7,584,003	3.7	360	-90	30
DC-293	RAB	686,573	7,583,954	3.7	360	-90	25
DC-294	RAB	686,572	7,583,906	3.7	360	-90	55
DC-PDH1	RC	685,910	7,584,367	19.0	360	-90	560
DC-PDH2	RC	685,859	7,583,643	50.0	360	-90	300
DC-PDH3	RC	687,322	7,583,560	58.0	360	-90	45
DC-PDH4	RC	685,767	7,584,453	50.0	360	-90	1,600
DC-PDH5	RC	684,890	7,583,544	66.0	0	-90	0
DC-PDH6	RC	684,823	7,583,606	66.0	0	-90	0
DEN-1	Diamond	686,235	7,584,563	100.0	360	-90	1,800
DEN-2	Diamond	686,260	7,584,763	50.0	360	-90	1,600
FC-0000	RAB	689,418	7,583,867	3.7	360	-90	55
FC-0200	RAB	689,407	7,583,670	3.7	360	-90	5
FC-0400	RAB	689,408	7,583,470	3.7	360	-90	80
FC-0600	RAB	689,401	7,583,272	3.7	360	-90	100
FC-1000	RAB	689,389	7,582,880	3.7	360	-90	40
FC-1200	RAB	689,389	7,582,682	3.7	360	-90	30
PT-0000	RAB	691,086	7,582,992	3.7	360	-90	240
PT-0200	RAB	690,947	7,583,122	3.7	360	-90	25
PT-0400	RAB	690,808	7,583,264	3.7	360	-90	10
PT-0600	RAB	690,658	7,583,411	3.7	360	-90	10
PT-0800	RAB	690,516	7,583,547	3.7	360	-90	10
PT-1000	RAB	690,382	7,583,682	3.7	360	-90	5
PT-1200	RAB	690,240	7,583,821	3.7	360	-90	10
PT-1400	RAB	690,095	7,583,956	3.7	360	-90	2
TL-0000	RAB	686,570	7,584,618	3.7	360	-90	55
TL-0200	RAB	686,781	7,584,507	3.7	360	-90	320
TL-0400	RAB	686,986	7,584,397	3.7	360	-90	300
TL-0600	RAB	687,191	7,584,288	3.7	360	-90	350
TL-0800	RAB	687,397	7,584,174	3.7	360	-90	30
TL-1000	RAB	687,606	7,584,059	3.7	360	-90	30
TL-1200	RAB	687,797	7,583,956	3.7	360	-90	45
TL-1400	RAB	687,959	7,583,861	3.7	360	-90	10
TL-1600	RAB	688,133	7,583,768	3.7	360	-90	25
TL-1800	RAB	688,301	7,583,678	3.7	360	-90	20
TL-2000	RAB	688,445	7,583,600	3.7	360	-90	50
TL-2200	RAB	688,612	7,583,506	3.7	360	-90	35
TL-2400	RAB	688,787	7,583,410	3.7	360	-90	40
TL-2600	RAB	688,956	7,583,321	3.7	360	-90	35
TL-2800	RAB	689,092	7,583,254	3.7	360	-90	65
TL-3000	RAB	689,237	7,583,171	3.7	360	-90	35

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
TL-3200	RAB	689,337	7,583,094	3.7	360	-90	100
TL-3400	RAB	689,578	7,582,985	3.7	360	-90	80
TL-3600	RAB	689,763	7,582,884	3.7	360	-90	60
TL-3800	RAB	689,954	7,582,782	3.7	360	-90	65
TL-4000	RAB	690,128	7,582,686	3.7	360	-90	60
TL-4200	RAB	690,269	7,582,563	3.7	360	-90	130
TL-4400	RAB	690,405	7,582,421	3.7	360	-90	120
TL-4600	RAB	690,543	7,582,277	3.7	360	-90	75
TL-4800	RAB	690,682	7,582,136	3.7	360	-90	20
TL-5000	RAB	690,823	7,581,997	3.7	360	-90	20
TL-5200	RAB	690,956	7,581,850	3.7	360	-90	45
TL-5400	RAB	691,095	7,581,717	3.7	360	-90	80
TL-5600	RAB	691,236	7,581,575	3.7	360	-90	15
TL-5800	RAB	691,378	7,581,427	3.7	360	-90	20
TL-6000	RAB	691,516	7,581,286	3.7	360	-90	50
TP01	RAB	690,654	7,583,110	3.7	360	-90	30
TP02	RAB	690,649	7,582,902	3.7	360	-90	135
TP03	RAB	690,639	7,582,693	3.7	360	-90	60
TP04	RAB	690,632	7,582,488	3.7	360	-90	10
TP05	RAB	690,628	7,582,275	3.7	360	-90	22
TP06	RAB	690,880	7,583,107	3.7	360	-90	80
TP07	RAB	690,869	7,582,898	3.7	360	-90	200
TP08	RAB	690,864	7,582,689	3.7	360	-90	90
TP09	RAB	690,856	7,582,486	3.7	360	-90	75
TP10	RAB	690,849	7,582,269	3.7	360	-90	20
TP11	RAB	691,091	7,583,101	3.7	360	-90	25
TP12	RAB	691,084	7,582,888	3.7	360	-90	0
TP13	RAB	691,081	7,582,681	3.7	360	-90	180
TP14	RAB	691,072	7,582,478	3.7	360	-90	100
TP15	RAB	691,068	7,582,266	3.7	360	-90	15
TP16	RAB	691,298	7,583,094	3.7	360	-90	80
TP17	RAB	691,293	7,582,883	3.7	360	-90	180
TP18	RAB	691,284	7,582,679	3.7	360	-90	170
TP19	RAB	691,278	7,582,474	3.7	360	-90	175
TP20	RAB	691,276	7,582,262	3.7	360	-90	70
TP21	RAB	691,512	7,583,091	3.7	360	-90	30
TP22	RAB	691,504	7,582,879	3.7	360	-90	180
TP23	RAB	691,500	7,582,677	3.7	360	-90	100
TP24	RAB	691,490	7,582,470	3.7	360	-90	175
TP25	RAB	691,484	7,582,256	3.7	360	-90	100
TP26	RAB	691,722	7,583,084	3.7	360	-90	40
TP27	RAB	691,715	7,582,876	3.7	360	-90	200
TP28	RAB	691,710	7,582,669	3.7	360	-90	140
TP29	RAB	691,701	7,582,465	3.7	360	-90	100
TP30	RAB	691,690	7,582,255	3.7	360	-90	135
TP31	RAB	691,900	7,583,077	3.7	360	-90	60

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
TP32	RAB	691,895	7,582,868	3.7	360	-90	10
TP33	RAB	691,882	7,582,664	3.7	360	-90	30
TP34	RAB	691,884	7,582,252	3.7	360	-90	130
TP35	RAB	692,086	7,583,077	3.7	360	-90	10
TP36	RAB	692,083	7,582,865	3.7	360	-90	35
TP37	RAB	692,071	7,582,659	3.7	360	-90	25
TP38	RAB	692,070	7,582,449	3.7	360	-90	30
TP39	RAB	692,065	7,582,239	3.7	360	-90	40
TP40	RAB	692,283	7,582,653	3.7	360	-90	5
TP41	RAB	692,495	7,582,647	3.7	360	-90	5
TP42	RAB	692,692	7,582,639	3.7	360	-90	25
TP43	RAB	692,903	7,582,635	3.7	360	-90	10
TP-PDH1	RC	691,080	7,582,682	50.0	360	-90	490
TP-PDH2	RC	691,882	7,582,664	50.0	360	-90	2,700
TP-PDH3	RC	691,642	7,582,646	50.0	360	-90	480
TP-PDH4	RC	691,307	7,582,848	52.0	360	-90	300
TP-PDH5	RC	691,065	7,582,991	28.0	360	-90	240
TP-PDH5B	RC	691,054	7,582,961	50.0	360	-90	170
TP-PDH6	RC	692,171	7,582,656	50.0	360	-90	1,700
W-01	Diamond	689,362	7,585,347	305.0	360	-90	5,200
W-02	Diamond	689,633	7,585,321	152.4	360	-90	3,900
W-03	Diamond	689,608	7,585,834	105.6	279	-60	1,200
W-04	Diamond	689,305	7,585,110	152.4	360	-90	3,400
W-05	Diamond	688,999	7,585,596	152.4	360	-90	3,300
W-06	Diamond	689,724	7,584,958	243.8	279	-60	7,000
W-07	Diamond	689,120	7,585,353	199.5	360	-90	3,300
W-08	Diamond	689,952	7,584,824	152.4	360	-90	4,500
W-09	Diamond	688,576	7,585,741	100.0	360	-90	1,200
W-10	Diamond	689,699	7,585,556	150.0	360	-90	1,200
W-11	Diamond	689,964	7,586,025	306.8	0	0	0
W-PDH1	RC	689,056	7,584,634	50.0	360	-90	1,500
W-PDH2	RC	689,689	7,585,798	50.0	360	-90	660
W-PDH3	RC	690,005	7,586,036	60.0	0	0	60,000
W-PDH4	RC	689,918	7,585,994	60.0	0	0	5,800
W-PDH5	RC	689,595	7,585,626	50.0	360	-90	2,600
W-PDH6	RC	689,466	7,585,702	50.0	360	-90	2,400
W-PDH7	RC	689,319	7,585,800	49.0	0	0	640
W-PDH8	RC	689,610	7,585,175	51.0	0	0	10,500
W-PDH9	RC	689,592	7,585,037	57.0	0	0	8,800
W-PDH10	RC	689,432	7,584,638	44.0	0	0	4,400
W-PDH11	RC	690,457	7,584,627	54.0	0	0	190
W-PDH12	RC	690,312	7,584,576	80.0	0	0	3,200
W-PDH13	RC	690,127	7,584,809	30.0	0	0	2,800
W-PDH13A	RC	690,116	7,584,712	38.0	0	0	1,600
W-PDH14	RC	689,765	7,584,649	54.0	0	0	1,200
W-PDH15	RC	689,126	7,584,861	78.0	0	0	4,800

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
W-PDH16	RC	689,955	7,586,069	20.0	0	0	80
W-PDH17	RC	690,008	7,585,969	20.0	0	0	40
W-PDH18	RC	689,906	7,585,967	50.0	0	0	300
W-PDH19	RC	689,446	7,586,106	44.0	0	0	960
W-PDH20	RC	687,642	7,585,178	56.0	0	-90	640
WA-001	RAB	689,246	7,585,352	10.1	360	-90	1,120
WA-002	RAB	689,184	7,585,354	8.2	360	-90	1,800
WA-003	RAB	689,123	7,585,356	6.4	360	-90	1,730
WA-004	RAB	689,062	7,585,358	7.0	360	-90	1,460
WA-005	RAB	689,001	7,585,360	8.2	360	-90	2,100
WA-006	RAB	688,940	7,585,363	9.2	360	-90	1,920
WA-007	RAB	688,879	7,585,365	4.9	360	-90	820
WA-008	RAB	688,818	7,585,367	3.7	360	-90	875
WA-009	RAB	688,757	7,585,369	4.3	360	-90	730
WA-010	RAB	688,695	7,585,371	4.0	360	-90	670
WA-011	RAB	688,634	7,585,373	5.2	360	-90	470
WA-012	RAB	688,573	7,585,375	1.8	360	-90	730
WA-013	RAB	688,512	7,585,378	5.5	360	-90	890
WA-014	RAB	689,254	7,585,596	4.0	360	-90	1,850
WA-015	RAB	689,193	7,585,598	4.0	360	-90	660
WA-016	RAB	689,132	7,585,601	7.3	360	-90	520
WA-017	RAB	689,071	7,585,603	4.0	360	-90	920
WA-018	RAB	689,010	7,585,605	6.4	360	-90	1,980
WA-019	RAB	688,949	7,585,607	4.0	360	-90	2,500
WA-020	RAB	688,887	7,585,609	5.5	360	-90	1,900
WA-021	RAB	688,826	7,585,611	4.0	360	-90	1,200
WA-022	RAB	688,765	7,585,614	5.2	360	-90	620
WA-023	RAB	688,704	7,585,616	4.0	360	-90	1,440
WA-024	RAB	688,643	7,585,618	8.8	360	-90	940
WA-025	RAB	688,582	7,585,620	4.0	360	-90	530
WA-026	RAB	688,521	7,585,622	4.0	360	-90	950
WA-027	RAB	688,460	7,585,624	4.0	360	-90	745
WA-028	RAB	688,398	7,585,626	4.0	360	-90	365
WA-029	RAB	688,337	7,585,629	3.1	360	-90	265
WA-030	RAB	688,276	7,585,631	4.0	360	-90	340
WA-034	RAB	689,079	7,585,847	4.0	360	-90	830
WA-035	RAB	689,018	7,585,849	4.0	360	-90	845
WA-036	RAB	688,957	7,585,852	3.1	360	-90	360
WA-037	RAB	688,896	7,585,854	4.0	360	-90	2,200
WA-038	RAB	688,835	7,585,856	4.0	360	-90	1,425
WA-039	RAB	688,774	7,585,858	4.0	360	-90	885
WA-040	RAB	688,713	7,585,860	4.0	360	-90	740
WA-041	RAB	688,652	7,585,862	4.0	360	-90	1,800
WA-042	RAB	688,590	7,585,864	4.0	360	-90	1,125
WA-043	RAB	688,529	7,585,867	4.0	360	-90	580
WA-044	RAB	688,468	7,585,869	4.0	360	-90	445

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
WA-045	RAB	688,407	7,585,871	4.0	360	-90	315
WA-046	RAB	688,346	7,585,873	4.0	360	-90	70
WA-047	RAB	688,285	7,585,875	4.0	360	-90	500
WA-048	RAB	688,224	7,585,877	4.0	360	-90	150
WA-049	RAB	688,163	7,585,880	2.7	360	-90	120
WA-052	RAB	689,149	7,586,090	1.5	360	-90	580
WA-053	RAB	689,088	7,586,092	1.5	360	-90	445
WA-054	RAB	689,027	7,586,094	2.4	360	-90	610
WA-055	RAB	688,966	7,586,096	3.1	360	-90	245
WA-056	RAB	688,905	7,586,098	2.7	360	-90	500
WA-057	RAB	688,844	7,586,100	2.4	360	-90	1,175
WA-058	RAB	688,782	7,586,103	4.0	360	-90	310
WA-059	RAB	688,721	7,586,105	4.0	360	-90	340
WA-060	RAB	688,660	7,586,107	4.0	360	-90	295
WA-061	RAB	688,599	7,586,109	3.1	360	-90	255
WA-062	RAB	688,538	7,586,111	2.7	360	-90	80
WA-063	RAB	688,477	7,586,113	2.7	360	-90	180
WA-064	RAB	688,416	7,586,115	4.0	360	-90	1,950
WA-065	RAB	688,355	7,586,118	4.0	360	-90	15
WA-066	RAB	688,293	7,586,120	4.0	360	-90	25
WA-067	RAB	688,232	7,586,122	2.4	360	-90	40
WA-068	RAB	688,171	7,586,124	4.0	360	-90	80
WA-069	RAB	689,359	7,585,103	4.0	360	-90	1,420
WA-070	RAB	689,298	7,585,105	4.0	360	-90	830
WA-071	RAB	689,237	7,585,107	4.0	360	-90	685
WA-072	RAB	689,176	7,585,109	4.0	360	-90	1,520
WA-073	RAB	689,115	7,585,112	4.0	360	-90	1,280
WA-074	RAB	689,054	7,585,114	4.0	360	-90	0
WA-075	RAB	688,993	7,585,116	4.0	360	-90	565
WA-076	RAB	688,931	7,585,118	4.0	360	-90	695
WA-077	RAB	688,870	7,585,120	2.4	360	-90	880
WA-078	RAB	688,809	7,585,122	4.0	360	-90	920
WA-079	RAB	688,748	7,585,125	4.0	360	-90	925
WA-080	RAB	688,687	7,585,127	2.1	360	-90	890
WA-081	RAB	688,626	7,585,129	4.0	360	-90	3,200
WA-082	RAB	688,565	7,585,131	3.1	360	-90	155
WA-083	RAB	688,504	7,585,133	3.1	360	-90	65
WA-084	RAB	688,442	7,585,135	1.8	360	-90	295
WA-085	RAB	689,351	7,584,859	4.0	360	-90	935
WA-086	RAB	689,290	7,584,861	4.0	360	-90	560
WA-101	RAB	689,355	7,584,981	4.0	360	-90	1,940
WA-102	RAB	689,294	7,584,983	4.0	360	-90	550
WA-103	RAB	689,233	7,584,985	4.0	360	-90	820
WA-104	RAB	689,172	7,584,987	4.0	360	-90	1,750
WA-105	RAB	689,110	7,584,989	4.0	360	-90	1,720
WA-106	RAB	689,049	7,584,992	3.1	360	-90	825

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
WA-107	RAB	688,988	7,584,994	4.0	360	-90	745
WA-108	RAB	688,927	7,584,996	4.0	360	-90	695
WA-109	RAB	688,866	7,584,998	4.0	360	-90	365
WA-110	RAB	688,805	7,585,000	4.0	360	-90	350
WA-111	RAB	688,744	7,585,002	4.0	360	-90	200
WA-112	RAB	688,683	7,585,004	1.8	360	-90	205
WA-113	RAB	688,621	7,585,007	4.0	360	-90	625
WA-114	RAB	688,560	7,585,009	4.0	360	-90	560
WA-115	RAB	688,499	7,585,011	4.0	360	-90	576
WA-116	RAB	688,438	7,585,013	4.0	360	-90	520
WA-133	RAB	690,209	7,584,890	4.0	360	-90	1,175
WA-134	RAB	690,150	7,584,953	4.0	360	-90	525
WA-135	RAB	690,147	7,584,892	3.4	360	-90	855
WA-136	RAB	690,086	7,584,894	1.8	360	-90	605
WA-137	RAB	690,025	7,584,896	4.0	360	-90	2,300
WA-138	RAB	689,964	7,584,898	2.1	360	-90	880
WA-139	RAB	689,903	7,584,900	4.0	360	-90	655
WA-141	RAB	689,774	7,584,721	4.0	360	-90	1,850
WA-142	RAB	689,835	7,584,719	4.0	360	-90	1,450
WA-143	RAB	689,896	7,584,717	4.0	360	-90	725
WA-144	RAB	689,958	7,584,715	4.0	360	-90	480
WA-145	RAB	690,019	7,584,713	4.0	360	-90	980
WA-146	RAB	690,080	7,584,710	1.8	360	-90	205
WA-147	RAB	690,141	7,584,708	1.5	360	-90	145
WA-148	RAB	689,717	7,584,846	4.0	360	-90	865
WA-149	RAB	689,779	7,584,843	4.0	360	-90	865
WA-150	RAB	689,840	7,584,841	4.0	360	-90	1,450
WA-151	RAB	689,901	7,584,839	1.5	360	-90	335
WA-152	RAB	689,962	7,584,837	4.0	360	-90	4,220
WA-153	RAB	690,023	7,584,835	4.0	360	-90	2,300
WA-154	RAB	690,084	7,584,833	4.0	360	-90	4,300
WA-155	RAB	690,145	7,584,831	1.8	360	-90	170
WA-156	RAB	690,206	7,584,828	4.0	360	-90	870
WA-157	RAB	689,971	7,585,082	1.5	360	-90	205
WA-158	RAB	690,032	7,585,079	2.4	360	-90	225
WA-159	RAB	690,093	7,585,077	4.0	360	-90	360
WA-160	RAB	690,154	7,585,075	3.1	360	-90	340
WA-161	RAB	690,215	7,585,073	4.0	360	-90	615
WA-162	RAB	690,276	7,585,071	4.0	360	-90	605
WA-163	RAB	689,892	7,584,595	3.4	360	-90	975
WA-164	RAB	689,953	7,584,593	4.0	360	-90	375
WA-165	RAB	690,014	7,584,590	3.1	360	-90	245
WA-167	RAB	690,158	7,585,197	4.0	360	-90	500
WA-168	RAB	690,219	7,585,195	4.0	360	-90	1,050
WA-169	RAB	690,280	7,585,193	4.0	360	-90	255
WA-170	RAB	690,342	7,585,191	4.0	360	-90	160

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
WA-172	RAB	688,451	7,585,380	4.0	360	-90	1,125
WA-173	RAB	688,390	7,585,382	4.0	360	-90	975
WA-174	RAB	688,329	7,585,384	2.7	360	-90	705
WA-175	RAB	688,268	7,585,386	2.7	360	-90	700
WA-176	RAB	688,206	7,585,388	4.0	360	-90	520
WA-177	RAB	688,154	7,585,400	4.0	360	-90	440
WA-178	RAB	688,083	7,585,386	4.0	360	-90	305
WA-179	RAB	688,018	7,585,381	4.0	360	-90	430
WA-180	RAB	687,968	7,585,376	4.0	360	-90	710
WA-181	RAB	687,900	7,585,374	4.0	360	-90	465
WA-182	RAB	687,848	7,585,363	2.1	360	-90	380
WA-183	RAB	687,784	7,585,357	2.1	360	-90	230
WA-184	RAB	687,728	7,585,350	4.0	360	-90	1,425
WA-185	RAB	687,665	7,585,344	1.5	360	-90	685
WA-186	RAB	687,603	7,585,331	4.0	360	-90	640
WA-187	RAB	687,545	7,585,327	4.0	360	-90	470
WA-191	RAB	688,307	7,584,773	3.4	360	-90	100
WA-192	RAB	688,368	7,584,771	1.8	360	-90	155
WA-193	RAB	688,429	7,584,769	3.7	360	-90	100
WA-194	RAB	688,491	7,584,766	3.7	360	-90	125
WA-195	RAB	688,552	7,584,764	3.7	360	-90	50
WA-196	RAB	688,613	7,584,762	2.4	360	-90	170
WA-197	RAB	688,674	7,584,760	2.4	360	-90	175
WA-198	RAB	688,735	7,584,758	1.5	360	-90	130
WA-199	RAB	688,796	7,584,756	2.4	360	-90	225
WA-200	RAB	688,857	7,584,753	2.7	360	-90	140
WA-201	RAB	688,918	7,584,751	2.7	360	-90	475
WA-202	RAB	688,980	7,584,749	3.1	360	-90	170
WA-203	RAB	689,041	7,584,747	4.0	360	-90	370
WA-204	RAB	689,102	7,584,745	4.0	360	-90	795
WA-205	RAB	689,163	7,584,743	3.1	360	-90	2,000
WA-206	RAB	687,426	7,585,332	1.5	360	-90	260
WA-207	RAB	687,316	7,585,333	1.5	360	-90	175
WA-208	RAB	687,195	7,585,329	1.5	360	-90	130
WA-209	RAB	687,084	7,585,333	1.5	360	-90	415
WA-210	RAB	686,980	7,585,333	1.5	360	-90	465
WA-211	RAB	687,552	7,585,455	1.5	360	-90	460
WA-212	RAB	687,555	7,585,581	1.5	360	-90	595
WA-213	RAB	687,561	7,585,704	1.5	360	-90	680
WA-214	RAB	687,561	7,585,836	1.5	360	-90	280
WA-215	RAB	687,562	7,585,947	1.5	360	-90	120
WA-216	RAB	687,554	7,585,221	1.5	360	-90	190
WA-217	RAB	687,554	7,585,101	1.5	360	-90	195
WA-218	RAB	687,560	7,584,987	1.5	360	-90	190
WA-219	RAB	687,559	7,584,884	1.5	360	-90	165
WA-220	RAB	687,559	7,584,751	1.5	360	-90	125

Hole	Type	Easting	Northing	Depth	Azimuth	Dip	Max Cu ppm
WA-221	RAB	689,224	7,584,741	4.0	360	-90	1,070
WA-222	RAB	689,285	7,584,738	4.0	360	-90	1,240
WA-223	RAB	689,376	7,585,592	1.5	360	-90	245
WA-224	RAB	689,368	7,585,531	1.2	360	-90	295
WA-225	RAB	689,342	7,585,471	3.1	360	-90	3,600
WA-226	RAB	689,321	7,585,410	3.7	360	-90	3,500
WA-227	RAB	689,319	7,585,349	1.5	360	-90	2,300
WA-228	RAB	689,347	7,585,287	2.4	360	-90	2,360
WA-229	RAB	689,364	7,585,225	4.0	360	-90	3,200
WA-230	RAB	689,368	7,585,348	3.7	360	-90	1,800
WA-231	RAB	689,630	7,585,828	3.1	360	-90	465
WA-232	RAB	690,272	7,584,949	1.5	360	-90	195
WA-233	RAB	690,333	7,584,946	4.0	360	-90	215
WA-234	RAB	690,394	7,584,944	4.0	360	-90	165
WA-235	RAB	690,455	7,584,942	4.0	360	-90	185
WA-236	RAB	689,671	7,585,796	2.1	360	-90	320
WA-237	RAB	689,701	7,585,764	2.1	360	-90	540
WA-238	RAB	689,686	7,585,704	2.7	360	-90	290
WA-239	RAB	689,666	7,585,643	0.9	360	-90	490
WA-240	RAB	689,694	7,585,581	1.5	360	-90	175
WA-241	RAB	689,759	7,585,517	1.5	360	-90	135
WA-242	RAB	689,739	7,585,457	4.0	360	-90	330
WA-243	RAB	689,688	7,585,397	1.2	360	-90	70
WA-244	RAB	689,612	7,585,339	4.0	360	-90	615
WA-245	RAB	689,549	7,585,280	4.0	360	-90	3,700
WA-246	RAB	689,487	7,585,252	3.7	360	-90	2,100
WA-247	RAB	689,424	7,585,205	3.7	360	-90	1,350
WA-248	RAB	689,767	7,585,034	3.7	360	-90	750
WA-249	RAB	689,763	7,585,089	3.7	360	-90	1,480
WA-250	RAB	689,753	7,585,150	3.7	360	-90	1,925
WA-251	RAB	689,715	7,585,201	4.0	360	-90	680
WA-252	RAB	689,671	7,585,257	3.7	360	-90	465
WA-253	RAB	689,704	7,585,336	4.0	360	-90	580
WTDH001	Diamond	689,286	7,585,100	345.0	0	-60	2,488
WTDH002	Diamond	689,444	7,585,397	432.0	0	-60	12,077

Appendix 2 – Waitara historic drill intersections using a 0.2% Cu cut off, with a minimum width of 1 metre and including 3 metres of internal waste (MGA94 Zone 55)

Hole	East	North	From	To	Width	Cu %
W-01	689,362	7,585,347	8.0	10.0	2.0	0.37
W-01	689,362	7,585,347	24.0	40.0	16.0	0.25
W-01	689,362	7,585,347	46.0	70.0	24.0	0.31
W-01	689,362	7,585,347	74.0	86.0	12.0	0.43
W-01	689,362	7,585,347	92.0	136.0	44.0	0.29
W-01	689,362	7,585,347	144.0	158.0	14.0	0.26
W-01	689,362	7,585,347	166.0	168.0	2.0	0.20
W-01	689,362	7,585,347	174.0	182.0	8.0	0.24
W-01	689,362	7,585,347	192.0	194.0	2.0	0.23
W-01	689,362	7,585,347	200.0	214.0	14.0	0.26
W-01	689,362	7,585,347	220.0	222.0	2.0	0.28
W-01	689,362	7,585,347	226.0	228.0	2.0	0.27
W-01	689,362	7,585,347	240.0	242.0	2.0	0.20
W-01	689,362	7,585,347	246.0	248.0	2.0	0.24
W-01	689,362	7,585,347	260.0	270.0	10.0	0.33
W-01	689,362	7,585,347	274.0	276.0	2.0	0.29
W-01	689,362	7,585,347	280.0	282.0	2.0	0.20
W-02	689,633	7,585,321	41.0	43.0	2.0	0.30
W-02	689,633	7,585,321	47.0	49.0	2.0	0.20
W-02	689,633	7,585,321	61.0	63.0	2.0	0.22
W-02	689,633	7,585,321	75.0	92.0	17.0	0.23
W-02	689,633	7,585,321	112.0	114.0	2.0	0.21
W-02	689,633	7,585,321	116.0	118.0	2.0	0.22
W-02	689,633	7,585,321	132.0	150.0	18.0	0.23
W-04	689,305	7,585,110	10.0	12.0	2.0	0.24
W-04	689,305	7,585,110	18.0	24.0	6.0	0.25
W-04	689,305	7,585,110	28.0	32.0	4.0	0.27
W-04	689,305	7,585,110	50.0	54.0	4.0	0.28
W-04	689,305	7,585,110	58.0	60.0	2.0	0.26
W-04	689,305	7,585,110	64.0	68.0	4.0	0.22
W-04	689,305	7,585,110	78.0	80.0	2.0	0.20
W-04	689,305	7,585,110	94.0	96.0	2.0	0.20
W-04	689,305	7,585,110	102.0	108.0	6.0	0.21
W-04	689,305	7,585,110	116.0	118.0	2.0	0.21
W-04	689,305	7,585,110	128.0	130.0	2.0	0.27
W-04	689,305	7,585,110	146.0	148.0	2.0	0.20
W-05	688,999	7,585,596	32.1	38.7	6.6	0.27
W-05	688,999	7,585,596	44.0	46.7	2.7	0.22
W-05	688,999	7,585,596	53.0	55.0	2.0	0.22
W-05	688,999	7,585,596	58.4	60.5	2.1	0.20
W-05	688,999	7,585,596	71.0	73.0	2.0	0.21
W-05	688,999	7,585,596	75.0	79.0	4.0	0.20
W-06	689,712	7,584,960	21.0	29.0	8.0	0.45

Hole	East	North	From	To	Width	Cu %
W-06	689,703	7,584,961	35.0	49.0	14.0	0.28
W-06	689,649	7,584,970	151.0	153.0	2.0	0.21
W-07	689,120	7,585,353	18.0	22.0	4.0	0.27
W-07	689,120	7,585,353	26.0	34.0	8.0	0.23
W-07	689,120	7,585,353	38.0	42.0	4.0	0.23
W-07	689,120	7,585,353	48.0	50.0	2.0	0.20
W-07	689,120	7,585,353	52.0	54.0	2.0	0.26
W-07	689,120	7,585,353	76.0	88.0	12.0	0.25
W-07	689,120	7,585,353	92.0	102.0	10.0	0.25
W-08	689,952	7,584,824	9.0	18.0	9.0	0.23
W-08	689,952	7,584,824	34.0	36.0	2.0	0.23
W-08	689,952	7,584,824	44.0	78.0	34.0	0.26
W-08	689,952	7,584,824	90.0	94.0	4.0	0.21
W-08	689,952	7,584,824	98.0	106.0	8.0	0.30
W-08	689,952	7,584,824	122.0	124.0	2.0	0.23
W-08	689,952	7,584,824	144.0	146.0	2.0	0.26
W-PDH3	690,005	7,586,036	22.0	38.0	16.0	2.14
W-PDH3	690,005	7,586,036	54.0	56.0	2.0	0.25
W-PDH4	689,918	7,585,994	22.0	26.0	4.0	0.40
W-PDH4	689,918	7,585,994	30.0	32.0	2.0	0.35
W-PDH5	689,595	7,585,626	30.0	32.0	2.0	0.26
W-PDH6	689,466	7,585,702	36.0	38.0	2.0	0.24
W-PDH8	689,610	7,585,175	36.0	42.0	6.0	0.65
W-PDH9	689,592	7,585,037	30.0	34.0	4.0	0.21
W-PDH9	689,592	7,585,037	38.0	57.0	19.0	0.37
W-PDH10	689,432	7,584,638	32.0	36.0	4.0	0.41
W-PDH12	690,312	7,584,576	44.0	58.0	14.0	0.26
W-PDH13	690,127	7,584,809	8.0	12.0	4.0	0.25
W-PDH15	689,126	7,584,861	4.0	16.0	12.0	0.29
WA-019	688,949	7,585,607	1.2	4.0	2.7	0.24
WA-081	688,626	7,585,129	0.6	4.0	3.4	0.30
WA-137	690,025	7,584,896	2.7	4.0	1.2	0.23
WA-152	689,962	7,584,837	0.6	4.0	3.4	0.32
WA-153	690,023	7,584,835	2.7	4.0	1.2	0.23
WA-154	690,084	7,584,833	0.3	4.0	3.7	0.37
WA-205	689,163	7,584,743	1.5	3.0	1.5	0.20
WA-225	689,342	7,585,471	1.2	3.0	1.8	0.36
WA-226	689,321	7,585,410	1.5	3.7	2.1	0.35
WA-228	689,347	7,585,287	1.2	2.4	1.2	0.24
WA-229	689,364	7,585,225	1.5	4.0	2.4	0.32
WA-245	689,549	7,585,280	0.6	4.0	3.4	0.36
WA-246	689,487	7,585,252	0.6	3.7	3.0	0.21
WTDH001	689,286	7,585,109	15.0	21.0	6.0	0.25
WTDH001	689,286	7,585,140	28.0	130.0	102.0	0.22
WTDH001	689,286	7,585,232	255.0	273.0	18.0	0.24
WTDH002	689,444	7,585,398	1.0	4.0	3.0	0.20

Hole	East	North	From	To	Width	Cu %
WTDH002	689,444	7,585,427	11.0	110.0	99.0	0.35

Appendix 2 - JORC Code, 2012 Edition, Checklist of Assessment and Reporting Criteria

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary

Sampling techniques	• *Nature and quality of sampling (e.g., cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*
	• *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.*
	• *Aspects of the determination of mineralisation that are Material to the Public Report.*
	• *In cases where 'industry standard' work has been done this would be relatively simple (e.g., 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g., submarine nodules) may warrant disclosure of detailed information.*
		• One-metre primary samples were collected using a reverse circulation drill rig, which when split is approximately 10% of the total meter sample. The quality of the sample has been being actively measured using various quality control techniques, focusing on keeping holes dry, reducing dust loss and optimising sample delimitation. The quality of the sampling has been independently reviewed and is deemed to be high, and fit-for-purpose to be used in mineral resource estimations. Various quality control metrics are actively monitored to ensure the quality of samples collected. Such measures include:
		  ◦ Every effort is made to ensure all samples are drilled dry and when this is not possible samples are logged as wet, and the quality designation ranking lowered and considered in the resource estimation.
		  ◦ The measuring and monitoring of total RC sample weights to measure total recovery and metre delineation of the drilling (after correcting for density based on lithology averages and volume differences based on bit size)
		• pXRF analysis for some alteration and common rock-forming elements was carried out on every metre by taking a small ~25g sample from the bulk RC sample and analysing using an Olympus Vanta M series XRF Analyser with all three beams enabled with each beam set to 10 seconds each.
		• Calibration checks were performed by the handheld XRF analysers at least once fortnightly to ensure that the analyser was operating within factory specifications

Drilling techniques	• *Drill type (e.g., core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g., core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Reverse circulation drilling equipment with face sampling hammers were used to collect samples. The drilling was conducted by a McCulloch DR 800 drill rig with Sullair 350/1100 compressor, a Mercedes powered 350/1100 Sullair compressor. Boosters is a Detroit 8V92 type 650 psi to a maximum of 900psi. All drill bits used were face sampling Schramm 650 series 143 mm, had a shroud size of 141 mm, and they were sized to suit as they wore. Teeth are 8 PCD outer and 9 tungsten inner teeth. All rods were Manutech Rods which are 6 metres long 4 inch outside diameter. All sample hoses are 3 inch Inside diameter.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• All sample recovery information was digitally recorded on the rig using locked auto-validating excel spreadsheets. Samples were weighed using digital scales and recoveries were estimated based on average density of logged lithology, bit diameter (indicating volume of sample) and total sample weight. The recovery was constantly monitored using live-updating graphs indicating when recoveries were out of control or showing unfavourable trends. • An auxiliary booster was used to maximise air pressure to improve sample recovery, which allowed holes to be drilled dry. Where samples were drilled wet they have been logged as such. Furthermore, constant monitoring of recoveries via measurement and evaluation of total sample weights on the rig enable recoveries to be maximised.

Criteria	JORC Code explanation	Commentary
		• There is no relationship between sample recovery and grade and no correction or weighting factors were required.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Chip samples have been geologically and geotechnically logged to a level of detail to support mineral resource estimation, mining studies and metallurgical studies. All chip samples have been geologically logged to 1m resolution on the rig recording information on rock type, mineralogy, mineralisation, fabrics, and textures. This logging is paired with logging conducted using the downhole Televiewer information which can log to at least 10cm resolution and records structural information for contacts, foliation, banding, veining etc. in the form of dip and dip direction measurements., resistivity, natural gamma and density measurements are also used to assist this logging. • The logging for the RC drilling was qualitative for the geological data collection and quantitative for structural, geotechnical and geochemical data. A handheld XRF was used to collect continuous geochemical data and Televiewer optical and acoustic data collection allows the measurement of structural and geotechnical data. • All one metre samples from the drilling have been geologically logged and the geological data recorded in the drill database. Subsamples were also collected and stored in chip trays for future reference.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• All other samples were split using a cone splitter fixed to the side of the drill rig, a device aimed at reducing splitting variance. Holes were kept dry wherever possible using an auxiliary booster. The cone Splitter is able to deal with wet samples without introducing bias. This has been independently reviewed and is considered an appropriate technique to collect large-volume samples when extractor, delimitation and preparation errors are well managed. • For this project, the quality assurance and quality control on the primary calico sample were excellent, resulting in good metre delineation, minimal sample loss and good water management. • RC drill chips were delivered to a cone splitter, then weighed on receipt at the laboratory and dried in an LPG oven for 24hrs @ 95° C. Samples to 3kg are full pulverised to 85% passing 75µm in a FLSmidth LM5 mill. Samples >3kg are spilt 50:50 using a 25mm aperture riffle splitter prior to pulverising. Samples were then scooped from the LM5 bowl and put into brown paper bags, after which the final charge weight was prepared by scooping from the bag using a spoon. • The quality of the sampling preparation has been discussed in the announcement text and is considered of very good quality, supported by sufficient quality control data (duplicates). The techniques have all been independently reviewed and are all considered appropriate and fit for purpose. • The sample size is considered appropriate for the mineralisation style.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g., standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e., lack of bias) and precision have been established.*	• The nature of the laboratory processes has been discussed in the announcement text in more detail. The total 50g fire assay technique with aqua regia digest and AAS finish is considered appropriate for Au analysis. ME-ICP was used to analyse a total of 33 elements, including Cu and Ag. When a sample returned a value exceeding the analysis limit of Cu or Ag, the sample was re-analysed using an ore grade analysis method to accurately define the final analysis grade. The quality was carefully controlled by both Duke and ALS. • A pXRF Vanta m-series analysed each sample using 3 beams in geochemistry mode. Each beam was set to 10

Criteria	JORC Code explanation	Commentary
		seconds for a total of 30 seconds and targeting 39 elements, specifically anomalous copper. The pXRF Vanta m-series was calibrated once a week and the prolene pXRF windows were changed upon noticing any imperfection on the surface. A blank standard was analysed once a week or following the prolene window change. • QC samples were inserted in the form of Certified Reference Materials, blanks, crush duplicates and pulp duplicates. The results showed the laboratory delivered consistent results throughout the campaign. Bias and variance acceptance testing showed positive results, with the only issue noted the elevated variability in pulps.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• All significant intersections were inspected and verified by the Competent Person. • The data is collected via Duke Exploration Ltd's auto-validating, controlled spreadsheets with drop down menu entry. These sheets are loaded into an Access database using automatic scripting and are then subjected to a range of further tests for errors. Any issues were communicated to site within 24 hours and resolved before the data was accepted. The data is then validated within the database and brought into Micromine and further visual checks conducted. One database administrator conducts all data merging and storage into the database to ensure the integrity of the data. • No data has been adjusted.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• The drill holes have been accurately surveyed using a mmGPS in MGA 94/Zone 54. • Downhole survey data was collected using a North seeking solid state gyro during the downhole data acquisition. The gyro results were checked by the down hole surveyor by comparing them with the deviation data obtained with other down hole tools (OPTV and ATV) and by duplicating a total of three surveys. The location accuracy of sample data points is considered by the Competent person to be highly accurate and properly quality controlled. • Topographic control has been adopted from a recent aerial geophysical programme and has been corrected to height values from the DGPS survey. The topographic control is considered to be highly accurate.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• The drilling reported has been carried out on a 60mx60m grid. The holes are drilled to an average depth of around180m. • Geological and grade continuity has been confirmed across the 60m drill spacing. • No physical compositing of samples has occurred in this drilling.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• The drilling orientation has been determined via Televiewer structural interpretation and hole are oriented perpendicular to the main banding and foliation surface. Where the terrain is challenging the drill pads were moved along the line and the drill dip was steepened to intersect the drill target at depth. In these circumstances the drill intersection is not perpendicular to the geological structures or mineralisation. • There is no apparent bias in any of the drilling orientations used.
Sample security	• *The measures taken to ensure sample security.*	• All samples were removed from site on the day of drilling and stored inside a secure warehouse facility. The samples were transported by a certified freight company to ALS Laboratories. The samples are not left unattended

Criteria	JORC Code explanation	Commentary
		and a chain of custody is maintained throughout the shipping process.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• No audits have been conducted by external parties at this stage. Internal review by various company personnel has occurred.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• EPM 26499 'Bundarra' is located south of Nebo, QLD, and is held 100% by Duke Exploration Ltd. Parts of the tenement have native title interests with the Barada Barna people. • No known impediments.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• Production at Mt Flora began in the 1880s. Numerous shafts, to a maximum depth of 38 m, adits and surface workings were developed. Mining continued during the 1970s. Exploration since the 1960s included geological mapping (Endeavour Oil 1974-75) soil surveys (CRA Exploration 1962, Endeavour Oil 1974-75, Regency Resources 2005), rock chip sampling (Endeavour Oil 1974-75, Chesterfield Mining and Exploration 1983, Elliot Exploration 1987, Dominion Gold Operations 1991, Queensland Metals Corporation 1994), Geophysics (magnetics by Planet Metals in 1967 and Elliot Exploration 1987, gravity by Carpentaria Gold in 1984, IP by Endeavour Oil in 1975, and VTEM by Regency in 2014). Endeavour Oil drilled six diamond drillholes in 1975, and Queensland Metals Corporation drilled two percussion holes in 1994. Endeavour Oil 1974-75 carried out trial underground mining, metallurgical test work and resource estimation. Endeavour Oil did extensive work at Mt Flora from 1974-76, including detailed 1:500 scale mapping, rock chip sampling, geophysics, drilling and extending adits and shaft sinking. Petrology was done on ore material taken from the base of a shaft sunk on the Flora lode in 1972 (Endeavour Oil, 1974). Near surface narrow lode mineralisation was detected in the Mt Flora area using IP geophysics, and Endeavour Oil considered IP to be a useful reconnaissance tool. Six diamond holes were drilled to successfully test IP anomalies at depth. In 1974-75 Endeavour Oil undertook a mining exploration programme and used this work to complete a resource estimate for the Mt Flora lodes. • Elliot Exploration re-assayed the Endeavour Oil core for gold in 1987. In 1994 Normandy drilled two holes: MFP 01 and MFP 02 near the top of Mt Flora, and Regency Mines 2001-2013 did mapping and soil sampling, and apparently drilled RC holes in 2001, although no data were reported.
Geology	• *Deposit type, geological setting and style of mineralisation.*	• Copper, gold, silver and molybdenum mineralisation at Mt Flora is located within 300 m of the contact zone between the Bundarra Granodiorite and Back Creek Group sediments. In the Mt Flora area, shale,

Criteria	JORC Code explanation	Commentary
		siltstone and sandstone has been contact metamorphosed to an andalusite hornfels. Mineralisation at Mt Flora occurs in structurally controlled lodes, which crosscut the granodiorite-sediment contact, with mineralisation occurring on both sides of the contact. Mineralisation is hosted by faults and fractures, associated with sheeted quartz veins, hematite, limonite and pyrite. The lodes have massive sulphides with high copper percentages (>10%). Silver and zinc are present, as well as molybdenum and gold.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* o *easting and northing of the drill hole collar* o *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* o *dip and azimuth of the hole* o *down hole length and interception depth* o *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• See Table 1 in the main text.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g., cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• No data aggregation methods have been used in this announcement.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g., 'down hole length, true width not known').*	• The mean copper-mineralised vein direction is 40/099, while the drillholes were 55/270. This means the drillholes are close to perpendicular to the mean vein direction, and true widths are close to intercept lengths. This will vary on an individual basis. Where the terrain is challenging the drill pads where moved along the line and the drill dip was steepened to intersect the drill target at depth. In these circumstances the drill intersection is not perpendicular to the geological structures or mineralisation.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and* • *appropriate sectional views.*	• See Table 1 and Figure 1 and Figure 2 in the main text.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All drill holes assays returned to date from the current drill programme have been reported.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• A desktop study was completed by Core Metallurgy Pty Ltd, using the most recent drill data and flotation test work results to perform an order-of magnitude assessment of processing and operating options for a mine at Mt Flora. The goal of the study was to produce indicative flowsheets and the associated capital and operating costs to subsequently evaluate the feasibility and economic

Criteria	JORC Code explanation	Commentary
		viability of producing a copper concentrate via conventional open pit mining and processing methods from deposits in the Bundarra project area. • The cost estimates provided within the review are of a preliminary nature and should have an expected accuracy range of 25% to 45%. Scoping test work to assess metallurgical processing options was conducted by Core in May and June 2019 and these data were used to constrain the review. • Key assumptions include all mining will be from an open-pit, throughput rate will be 500,000 tonnes per annum of sulphide ore, a concentrate grade for copper of 24% and silver of 398 g/t Ag, concentrate filter cake delivered to Mt Isa by road transport and a locally based drive in/out workforce is available at Mackay or in the surrounding area. • The study considered twelve processing options with the Base Case capital cost estimate for the supply and construction of a concentrator with a nominal capacity of 500,000 dry tonnes per annum to produce a saleable rougher copper concentrate is estimated at approximately A$56.3 million. • Order of magnitude operating costs for a greenfield EPCM and second-hand process plant, at A$31-34 per tonne, were significantly lower compared to Builder Owner Operator (A$47-51 per tonne) and Contract Crushing / Direct Shipped Ore (A$65-89 per tonne) options. • A copper cut-off grade of 0.2% Cu represents the economic cut-off grade for the project using the current copper price and cost estimates above.
Further work	• *The nature and scale of planned further work (e.g., tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Further work will include drilling other prospects (Quorn) around the Bundarra Pluton to test results returned from GAIP, MLEM and 3D IP geophysical surveys and pXRF soil surveys.